

Development needs and knowledge gaps of CESAR1 solvent

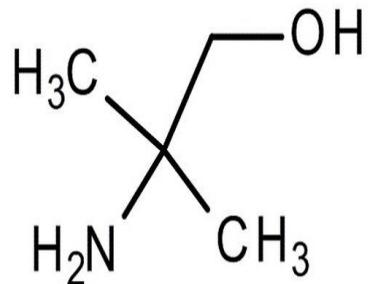
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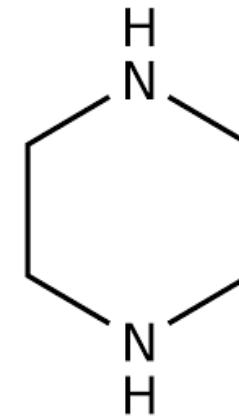
^b*SINTEF Industry, NO-7465 Trondheim, Norway*

Solvent Chemistry

CESAR1 is an aqueous amine-based solvent for CO₂ capture.



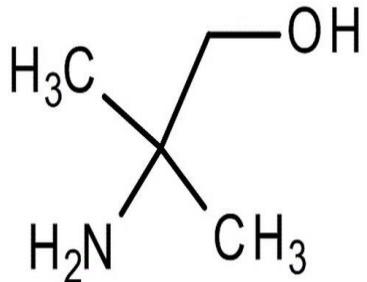
2-amino-2-methyl-1-propanol
(AMP)



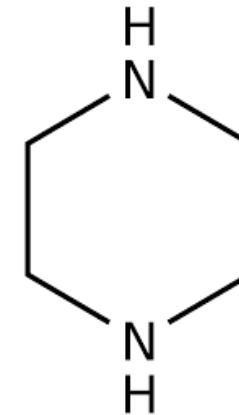
Piperazine
(PZ)

Solvent Chemistry

CESAR1 is an aqueous amine-based solvent for CO₂ capture.



2-amino-2-methyl-1-propanol
(AMP)



Piperazine
(PZ)

AMP = sterically hindered amine

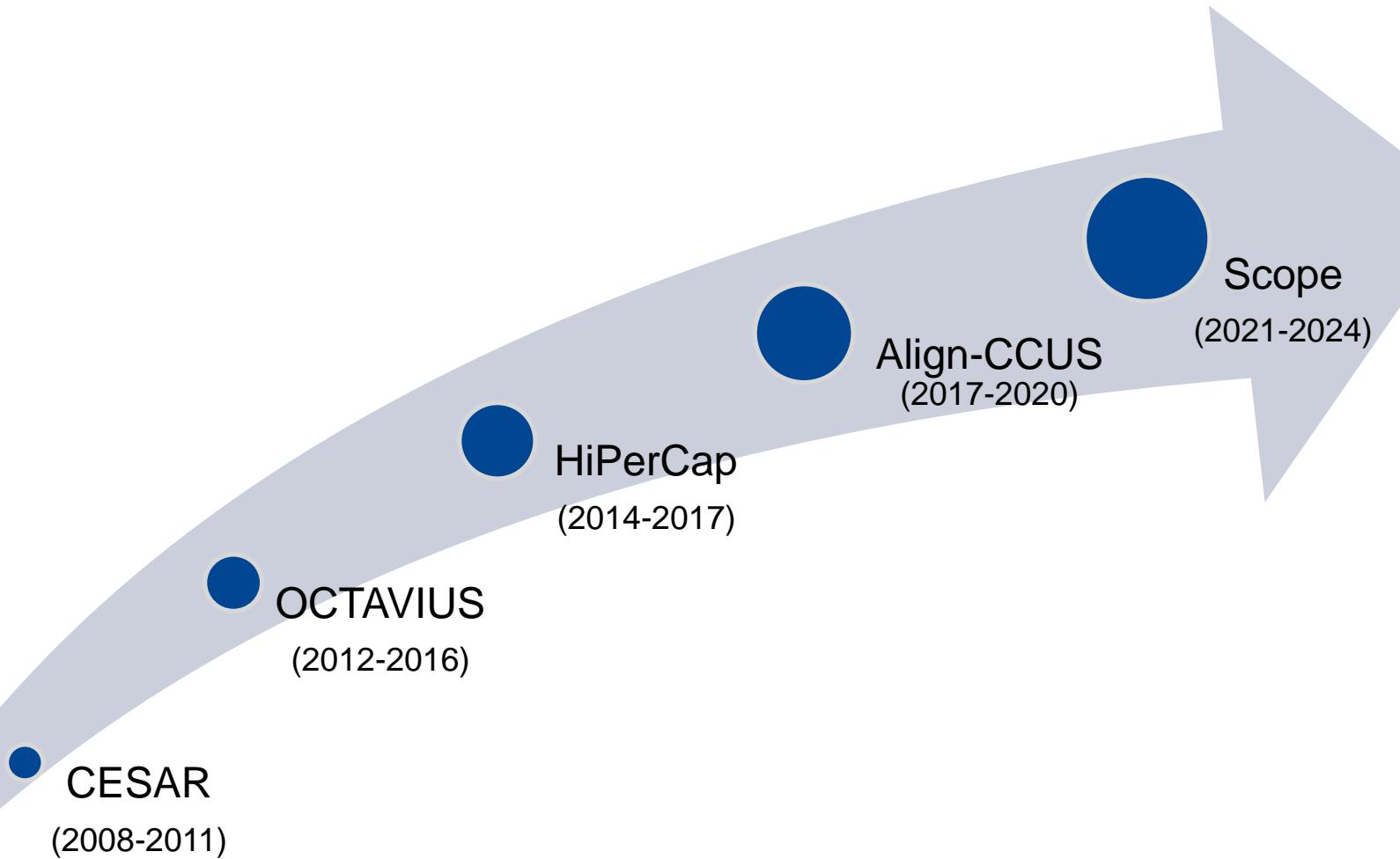
PZ = cyclic bifunctional amine.

CESAR1 is a blend of 3 M AMP and 1.5 M PZ

Why?

MEA vs CESAR1					
Energy Performance	Solvent Stability	Performance at high capture rate	Flexibility	Emission Control	Precipitation
					

History:



Nowadays and Scope of the work

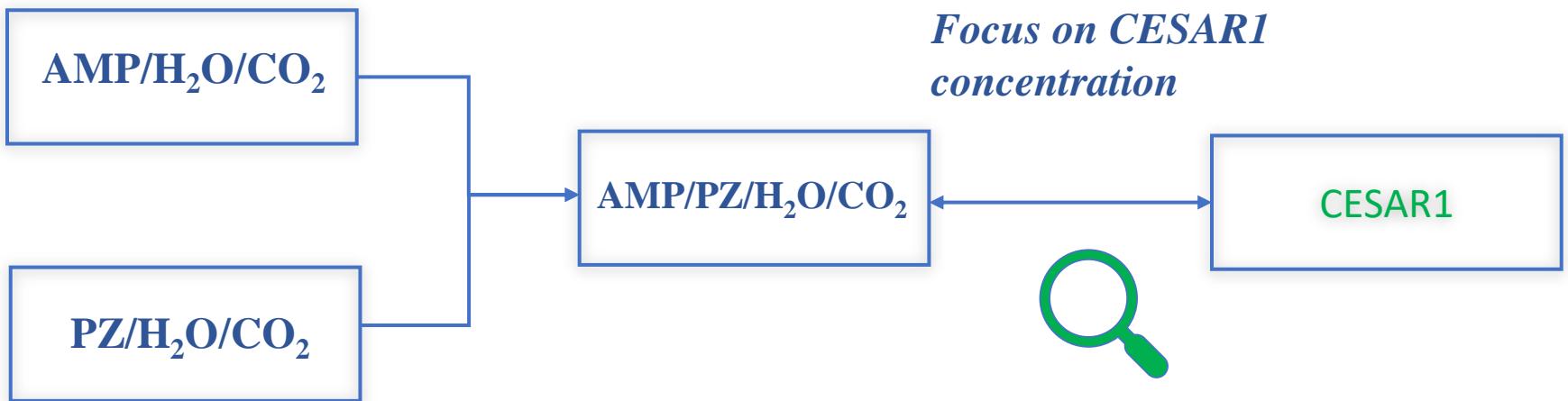


Mission: Development and qualification of CESAR1 solvent

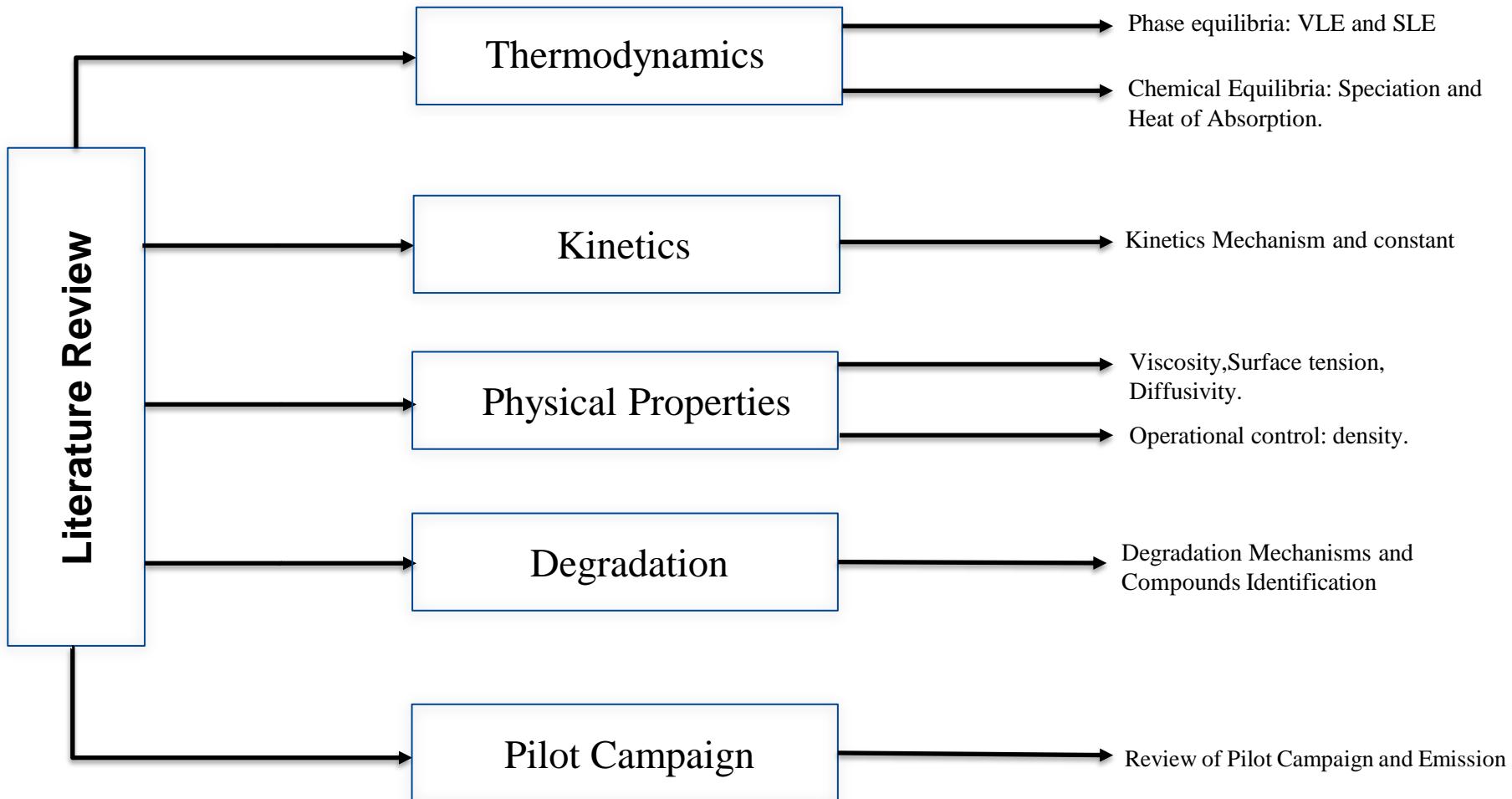


One of the milestones: *Filling the experimental gaps*

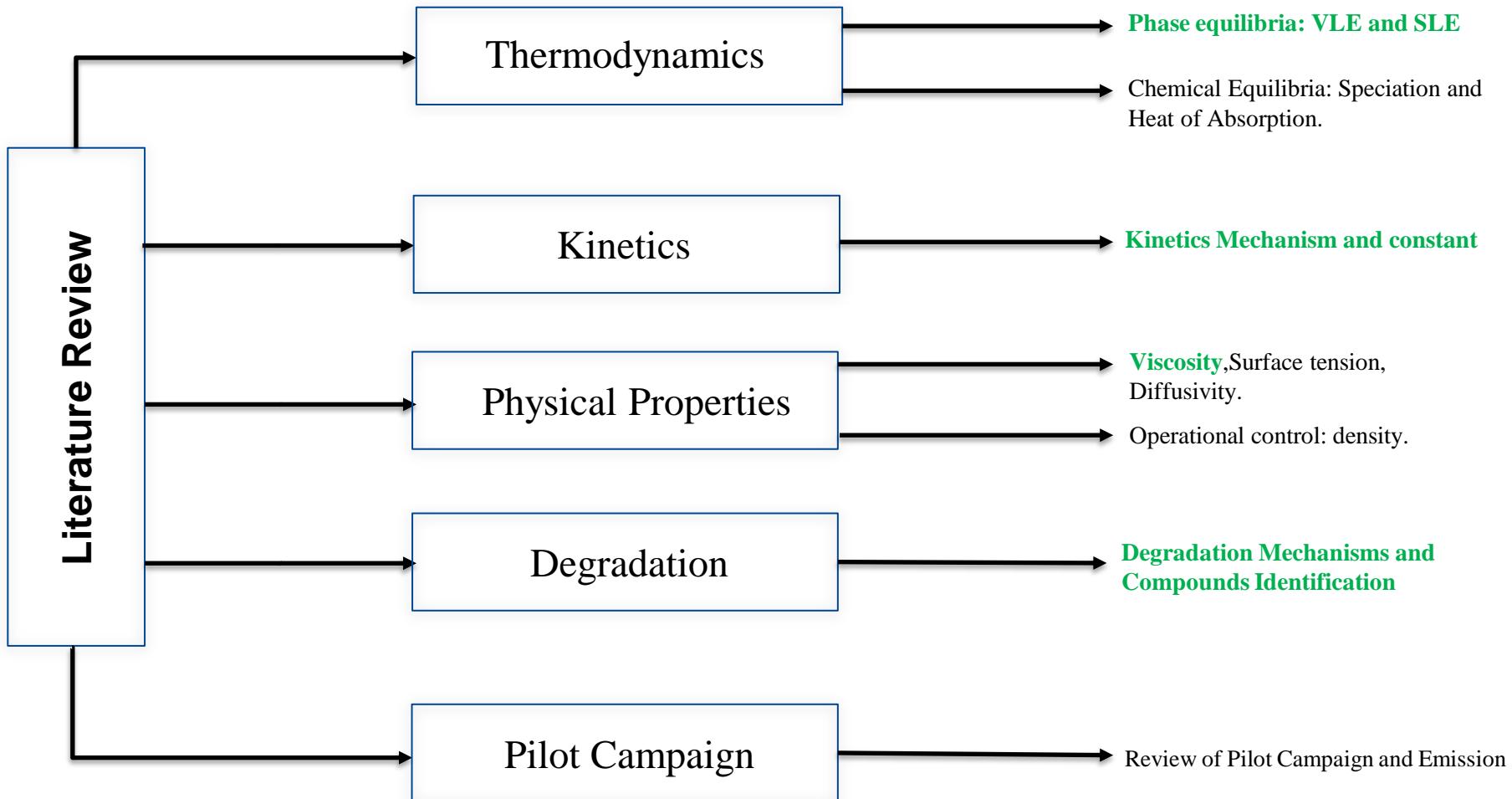
Methodology



Methodology



Outline



Thermodynamics: VLE for subsystems

AMP

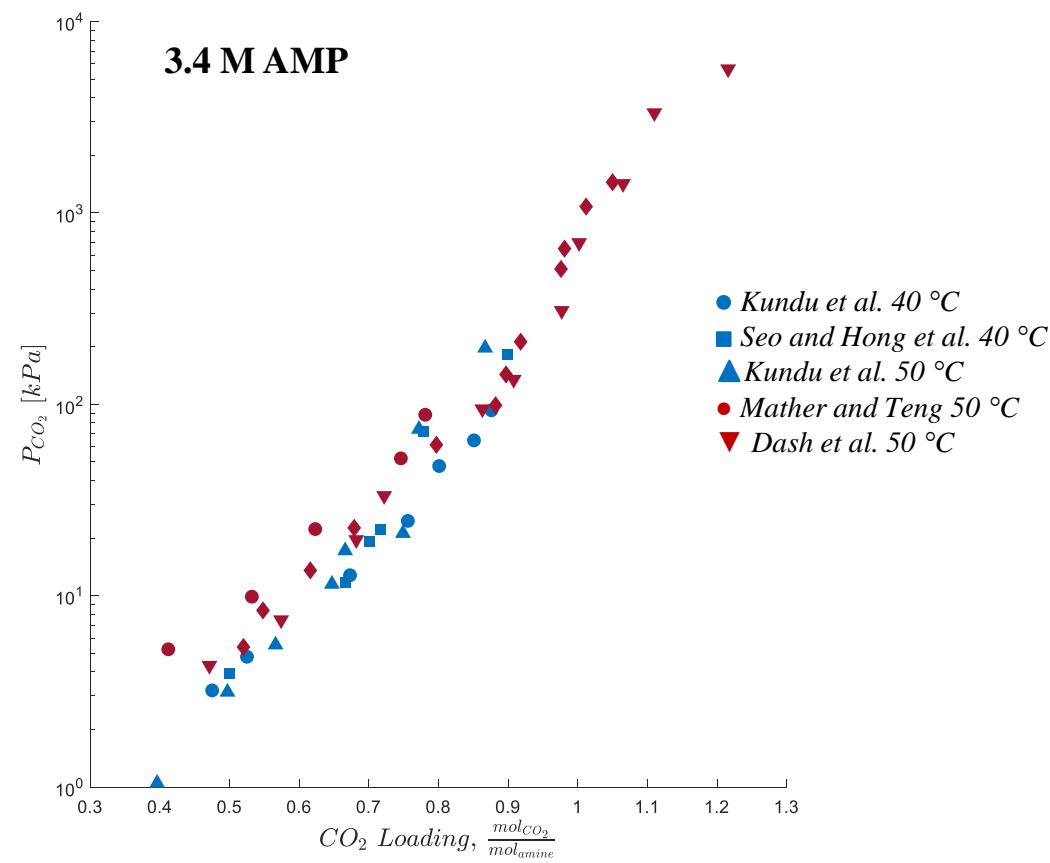
Concentration: from 0.1 M to 5.4 M AMP

Temperature: 20 up to 120 °C

PZ

Concentration: from 0.2 M to 4.9 M

Temperature: 20 up to 190 °C

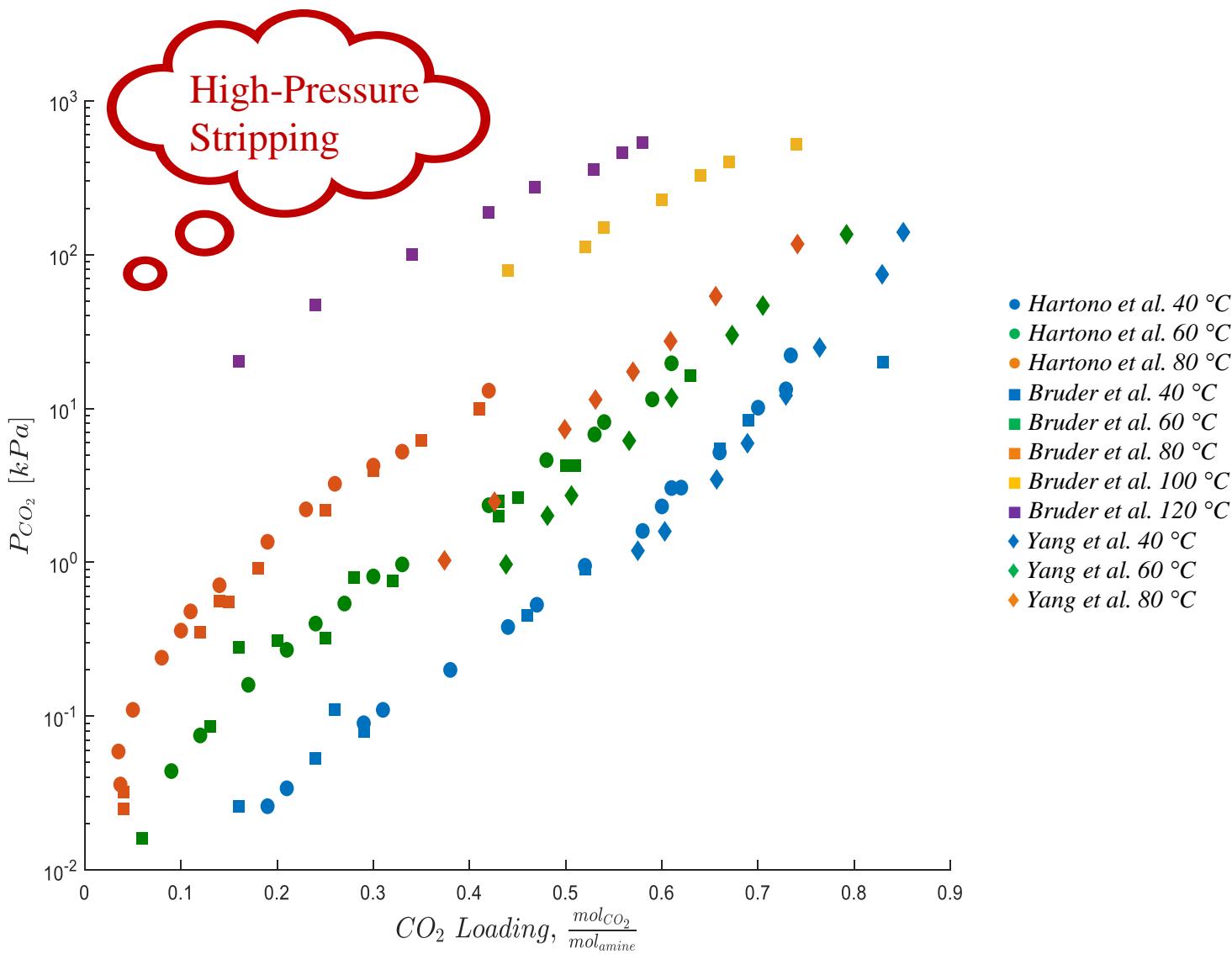


Some inconsistencies regarding
AMP VLE data at CESAR1
concentration have been found.

Thermodynamics: VLE for AMP/PZ

System	Experimental Range	Data Type	Instrument	Reference
AMP/PZ/H ₂ O/CO ₂	[AMP/PZ] = 3.0/1.5, 4.0/0.5,0.5/4.0,1.5/3.0,2.25/2.25 T = 40÷120 °C α_{CO_2} = 0.035÷1.05	P _{TOT} for T ≥ 100°C P _{CO₂}	Reaction Calorimetry and Vapor recirculation technique	Hartono, Ahmad, et al. (2021)
AMP/PZ/H ₂ O/CO ₂	[wf _{AMP} /wf _{PZ}] = 25/5,20/10 % T = 40÷120 °C α_{CO_2} = 0÷0.95	P _{TOT}	Static Analytical Apparatus	Tong et al. (2013)
AMP/PZ/H ₂ O/CO ₂	[m _{AMP} /m _{PZ}] = 2.3/5, 4/2 m T = 20÷160 °C α_{CO_2} = 0.268÷0.65	P _{CO₂}	Wetted Wall Column	Li et al. (2013)
AMP/PZ/H ₂ O/CO ₂	[wf _{AMP} /wf _{PZ}] = 38/2,35/5,32/8,45/5,42/8 % T = 30÷55 °C α_{CO_2} = 0.22÷1.03	P _{CO₂}	Equilibrium Cell	Dash et al. (2012)
AMP/PZ/H ₂ O/CO ₂	[AMP/PZ] = 3.0/1.5 T = 40÷120 °C α_{CO_2} = 0.04÷0.83	P _{CO₂}	Vapor Recirculation Technique	Brüder et al. (2011)
AMP/PZ/H ₂ O/CO ₂	[AMP/PZ] = 3.0/1.5 T = 40÷120 °C α_{CO_2} = 0.04÷0.83	P _{CO₂}	Vapor Recirculation Technique	Yang et al. (2010)

Thermodynamics: VLE for CESAR1



Thermodynamics: VLE Detected Gaps

1. Inconsistency for CO₂-solubility data for aqueous AMP solutions at CESAR1 concentration.
2. CO₂ Solubility data at temperature higher than 120 °C.
3. Vapor Liquid equilibrium data for diluted CESAR1 solvent.

Thermodynamics: SLE Detected Gaps

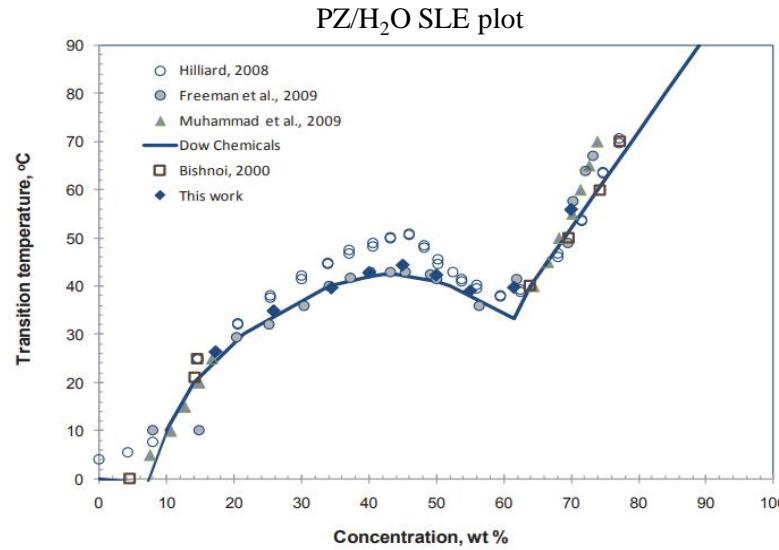
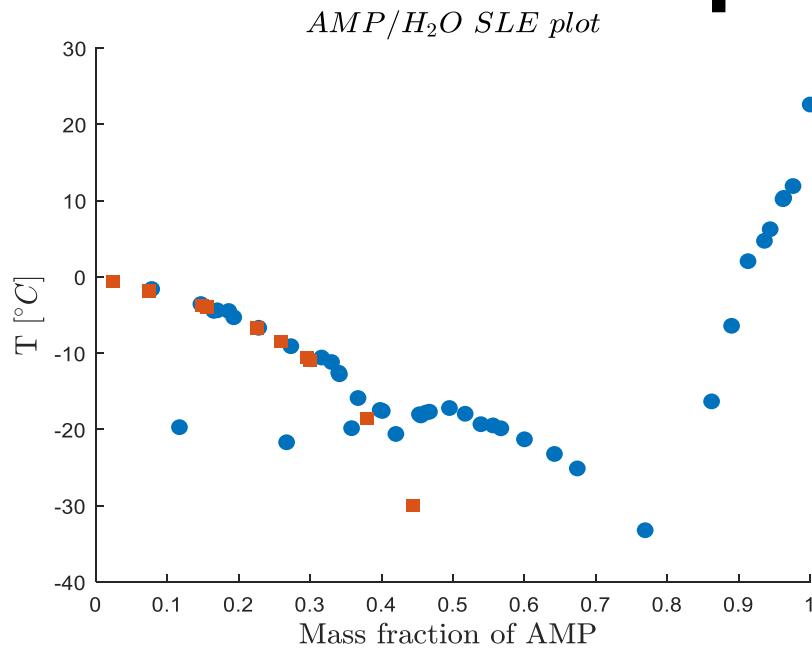
Formation of slurries and solids downstream may create unforeseen process conditions:

- Decrease equipment Efficiency
- Clogging
- Higher level of risk

- AMP Solid-Liquid Solubility Data ?

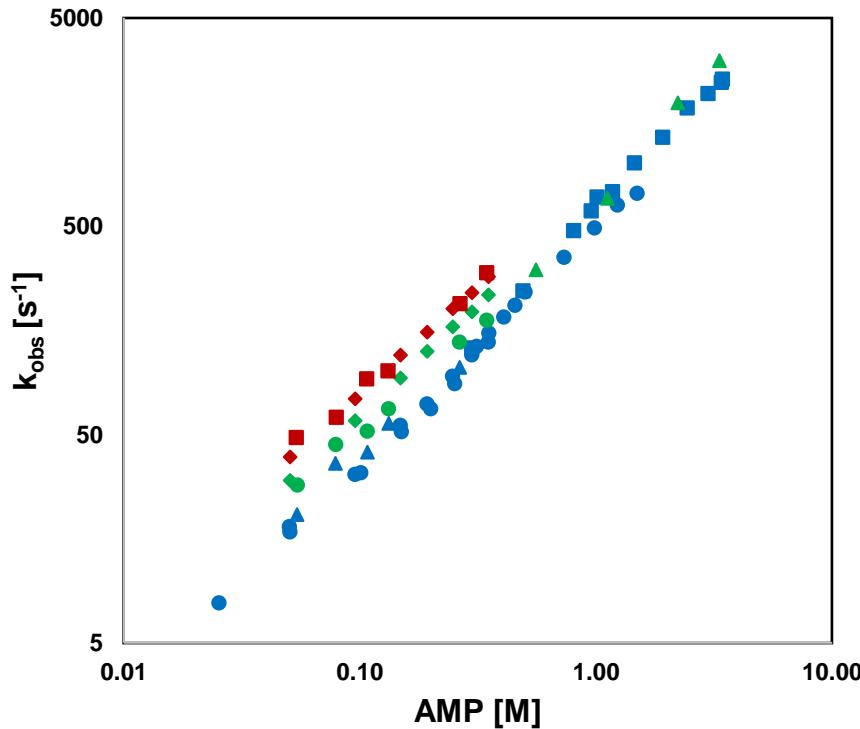
- PZ Solid-Liquid Solubility Data ✓

- AMP/PZ Solid-Liquid Solubility Data ?



Kinetics: AMP subsystem

AMP/H₂O/CO₂ Overall Kinetics Constant [s⁻¹]



First Order kinetics constant

$$r_{CO_2} = r_{CO_2-AMP} + r_{CO_2-OH^-}$$

$$r_{CO_2} = k_{2,AMP}[AMP][CO_2] + k_{OH^-}[OH^-][CO_2]$$

$$r_{CO_2} = (k_{2,AMP}[AMP] + k_{OH^-}[OH^-])[CO_2]$$

$$k_{obs} = k_{2,AMP}[AMP] + k_{OH^-}[OH^-]$$

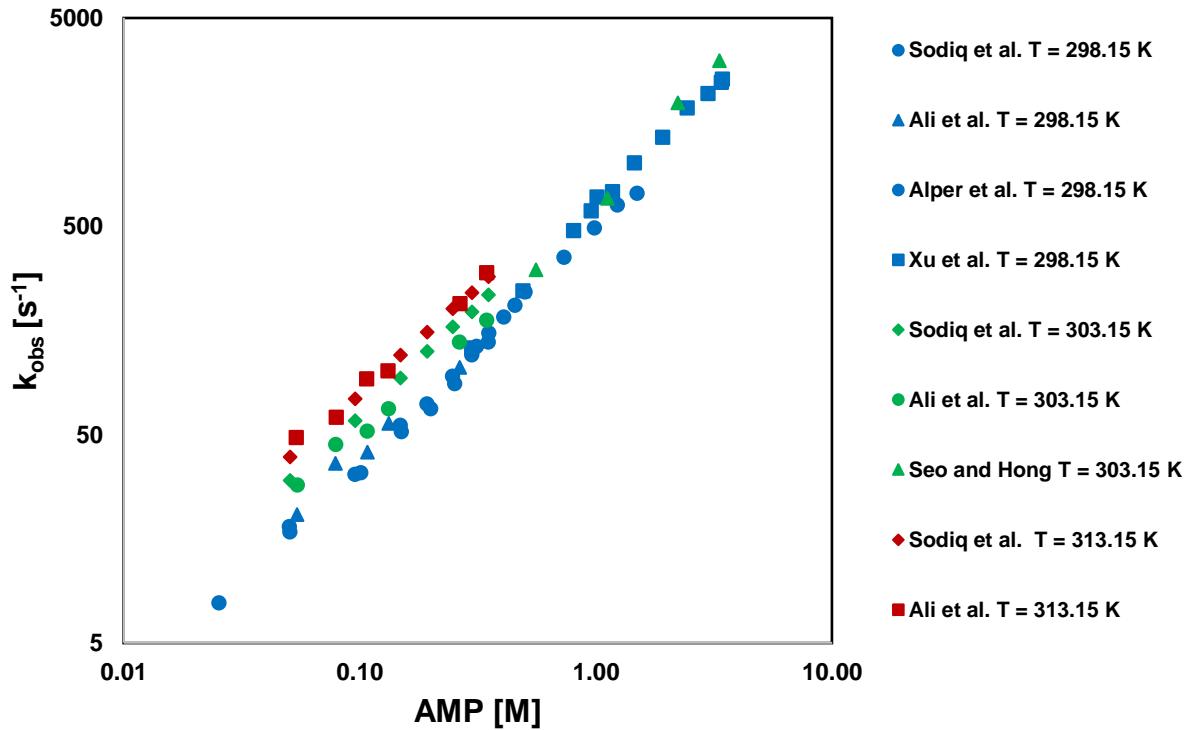
Steric hindrance

Kinetics Mechanism

Less basic due to α -Methyl substitutions

Kinetics: AMP subsystem

AMP/H₂O/CO₂ Overall Kinetics Constant [s⁻¹]



First Order kinetics constant

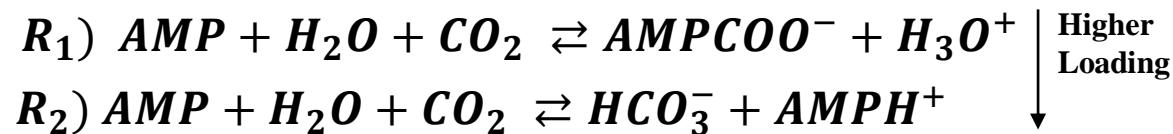
$$r_{CO_2} = r_{CO_2-AMP} + r_{CO_2-OH^-}$$

$$r_{CO_2} = k_{2,AMP}[AMP][CO_2] + k_{OH^-}[OH^-][CO_2]$$

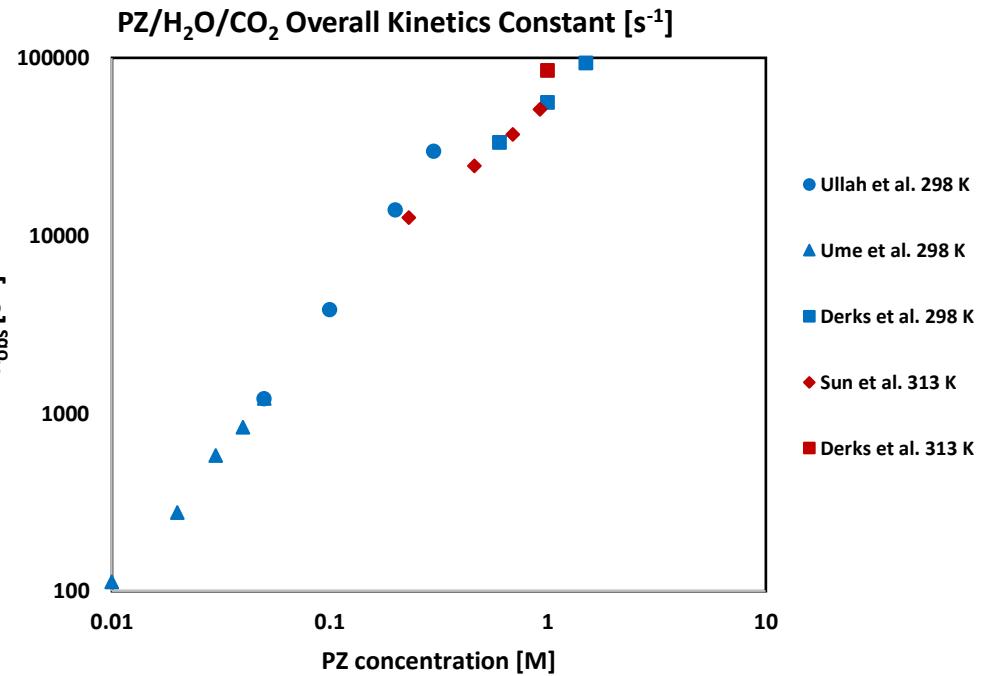
$$r_{CO_2} = (k_{2,AMP}[AMP] + k_{OH^-}[OH^-])[CO_2]$$

$$k_{obs} = k_{2,AMP}[AMP] + k_{OH^-}[OH^-]$$

CO₂ unloaded measurements!



Kinetics: PZ subsystem



First Order kinetics constant

$$r_{CO_2} = r_{CO_2-PZ} + r_{CO_2-OH^-}$$

$$r_{CO_2} = k_{2,PZ}[PZ][CO_2] + k_{OH^-}[OH^-][CO_2]$$

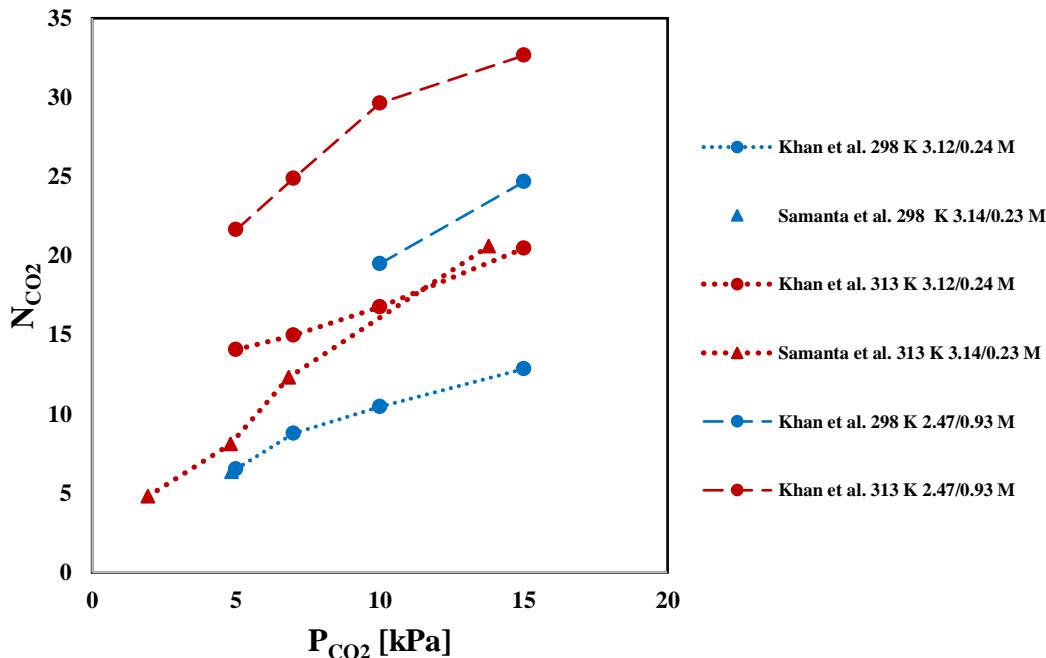
$$r_{CO_2} = (k_{2,PZ}[PZ] + k_{OH^-}[OH^-])[CO_2]$$

$$k_{obs} = k_{2,PZ}[PZ] + k_{OH^-}[OH^-]$$

Many data are available for CO₂-absorption kinetics in aqueous PZ solutions starting from CO₂-unloaded and CO₂-loaded solutions

Kinetics: AMP/PZ subsystem

AMP/PZ/H₂O CO₂ flux [kmol/m² s]



First Order kinetics constant

$$r_{CO_2} = r_{CO_2-PZ} + r_{CO_2-OH^-} + r_{CO_2-AMP}$$

$$r_{CO_2} = k_{2,PZ}[PZ][CO_2] + k_{OH^-}[OH^-][CO_2] + k_{2,AMP}[AMP][CO_2]$$

$$r_{CO_2} = (k_{2,PZ}[PZ] + k_{OH^-}[OH^-] + k_{2,AMP}[AMP])[CO_2]$$

$$k_{ov} = k_{2,PZ}[PZ] + k_{OH^-}[OH^-] + k_{2,AMP}[AMP]$$

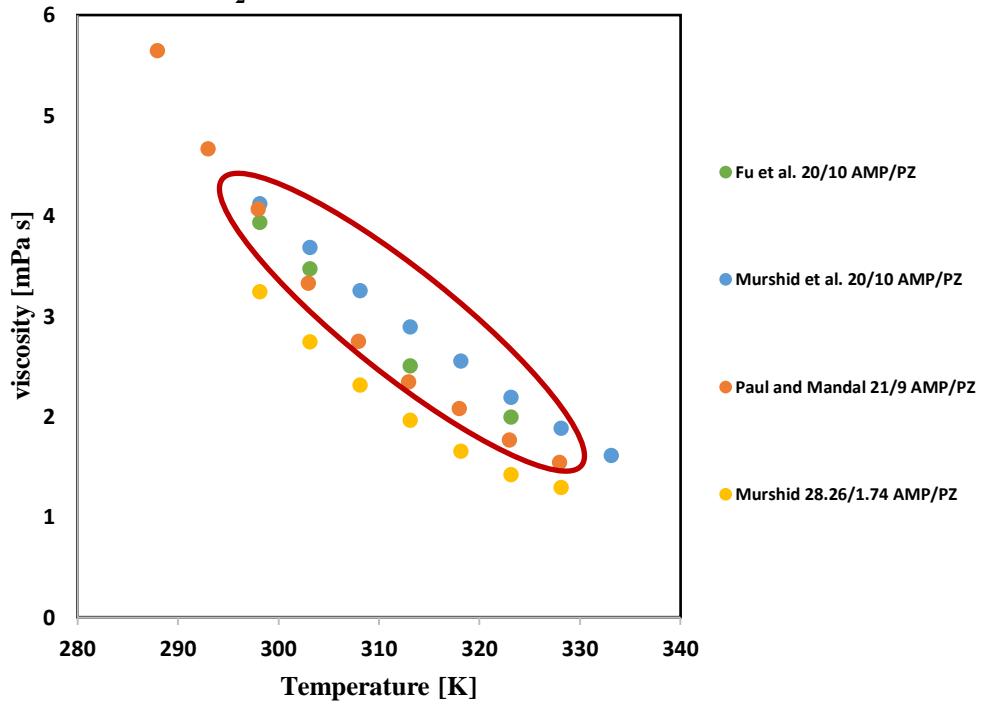
1. Data for blends available up to 1 M concentration of PZ.
2. Data available up to 40 °C.
3. Data available for CO₂-unloaded system.

Kinetics: Detected Gaps

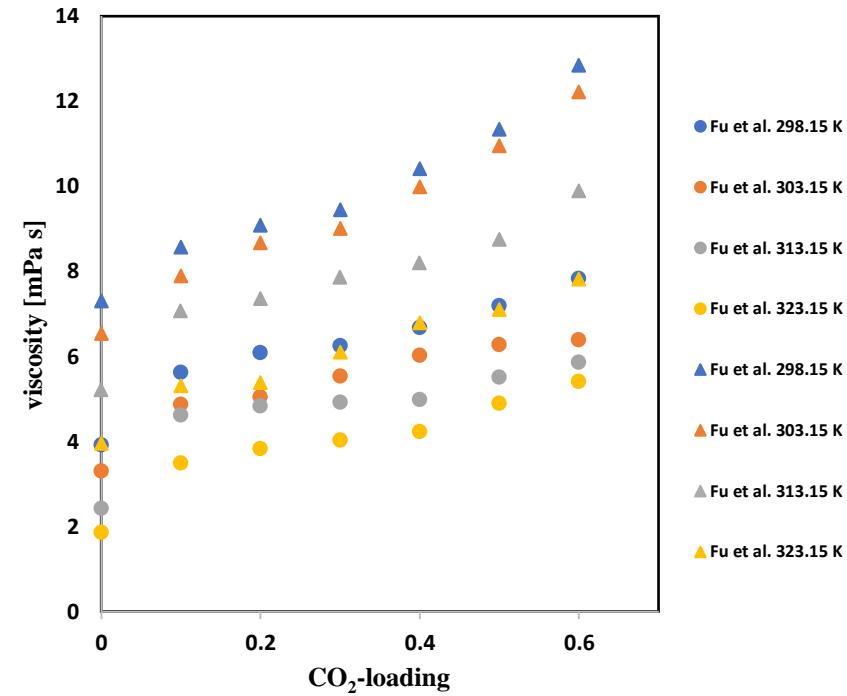
1. Measurements for CO₂-Loaded aqueous AMP solutions.
2. Measurements for CO₂-Loaded and CO₂-unloaded CESAR1 solutions are required
3. Extend temperature framework for blend kinetics measurements.

Viscosity: Detected Gaps

AMP/PZ/H₂O Unloaded solutions

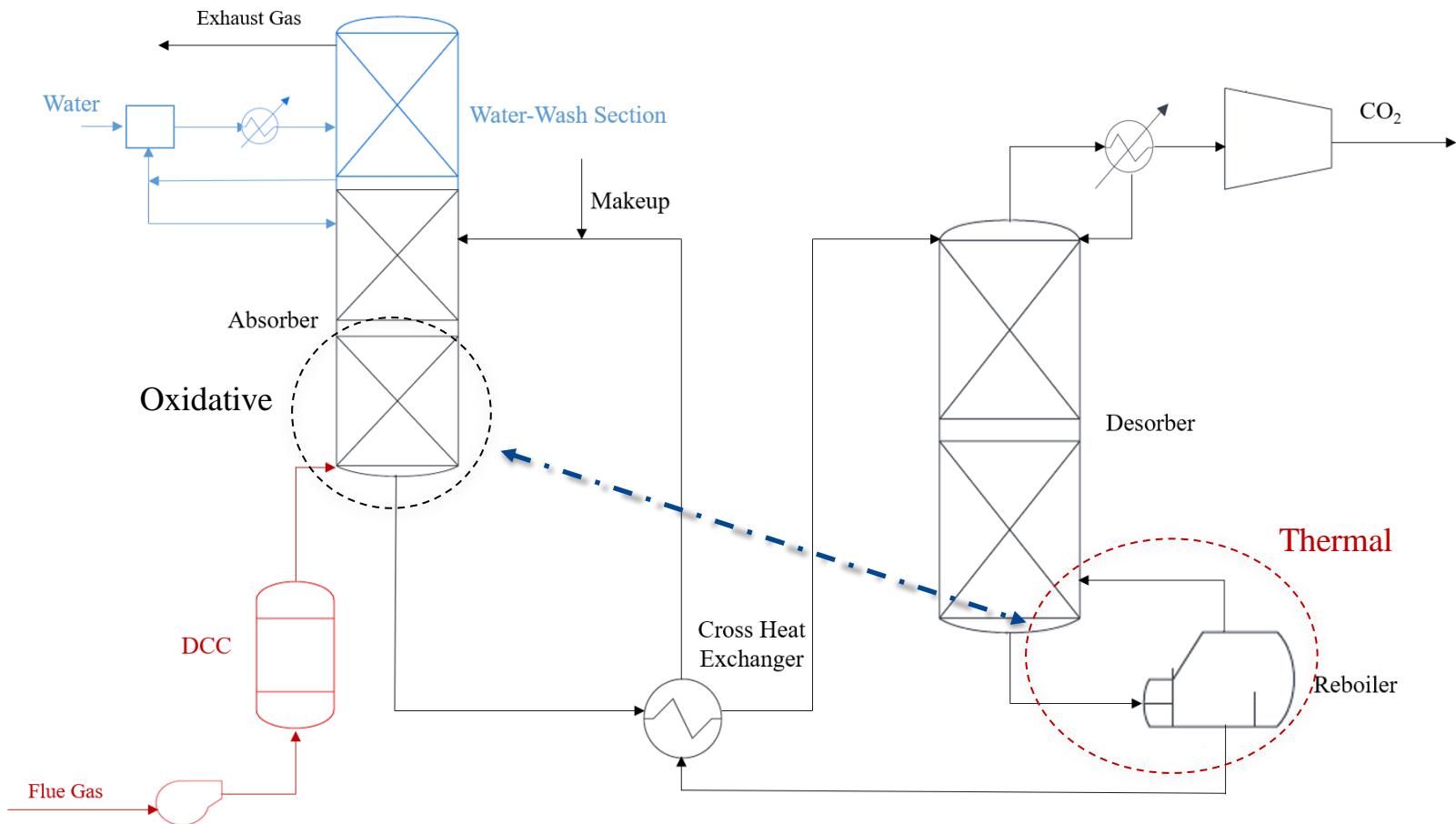


AMP/PZ/H₂O Loaded solutions: • 15/5 , ▲ 30/10 AMP/PZ wt%

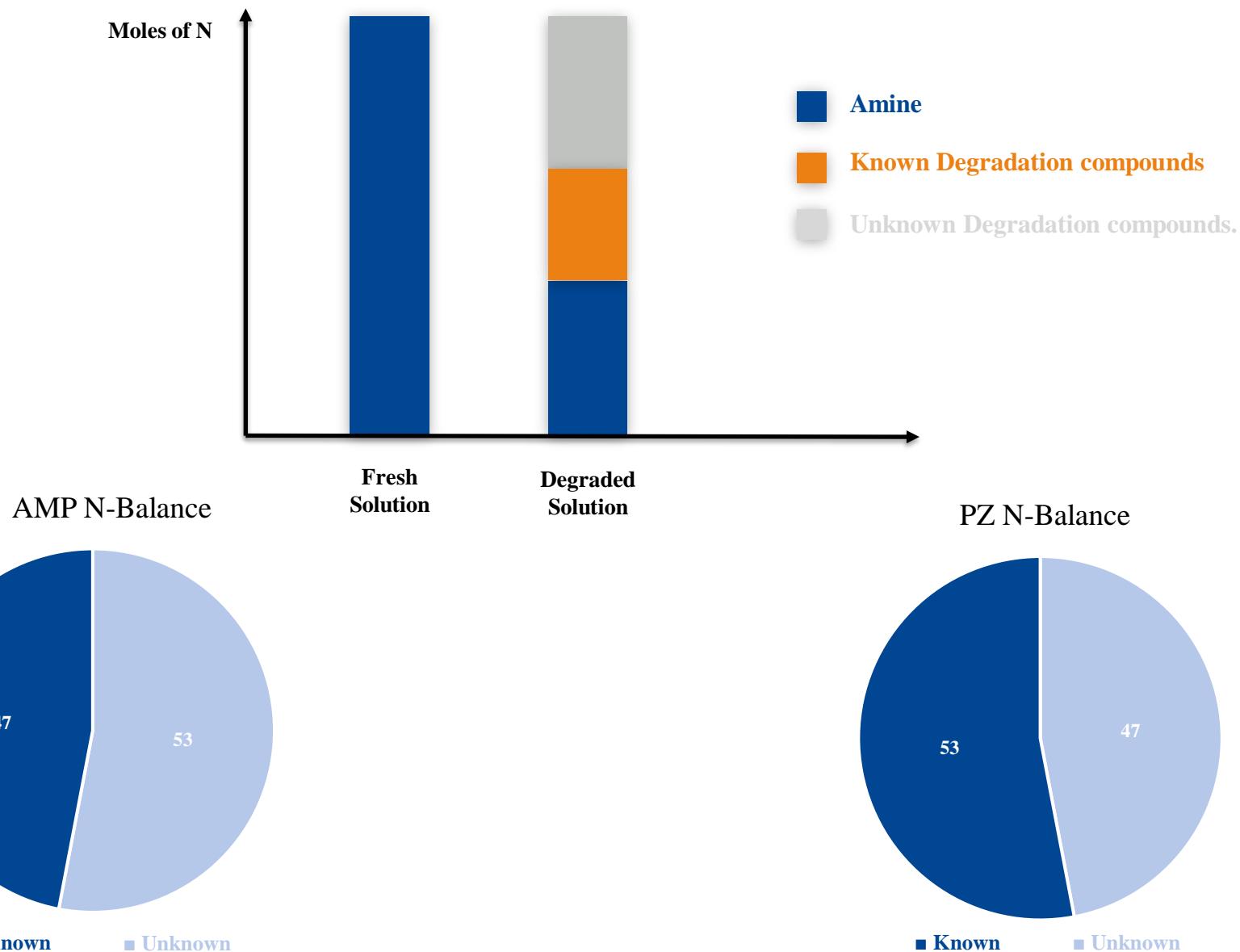


Data at CESAR1 concentration at CO₂-Loaded and CO₂-unloaded conditions are necessary

Amine Degradation



Degradation of AMP and PZ



Main Gaps Qualitative Review

Legend

Available

Gaps detected

Not available

Property	AMP/H ₂ O	PZ/H ₂ O	AMP/PZ/H ₂ O	AMP/H ₂ O/CO ₂	PZ/H ₂ O/CO ₂	AMP/PZ/H ₂ O/ CO ₂
Density	Available	Available	Available	Gaps detected	Not available	Gaps detected
Viscosity	Available	Available	Gaps detected	Not available	Available	Gaps detected
Diffusivity	Available	Gaps detected	Gaps detected	Not available	Not available	Not available
Kinetics	Available	Available	Gaps detected	Not available	Gaps detected	Not available
VLE	Available	Available	Available	Available	Available	Gaps detected
Speciation				Available	Available	Gaps detected
ΔH _{abs}				Available	Available	Available
\mathcal{H}	Available	Available	Gaps detected	Available	Not available	Not available
Degradation	Gaps detected	Gaps detected	Gaps detected	Gaps detected	Gaps detected	Gaps detected

QUESTIONS? Thank you!

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