

Amine Aerosol Characterization by FTIR and PDI in Pilot Plant Testing

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THE UNIVERSITY OF TEXAS AT AUSTIN
McKetta Department of
Chemical Engineering



Outline

Introduction

- Amine scrubbing
- Aerosol emissions

Analytical Methods

- Fourier Transform Infrared Spectrometry
- Phase Doppler Interferometry

Results

- Baghouse Pretreatment at NCCC
- SO₃ Generation at UT-SRP
- SO₃ Concentration Effect on Aerosol Emissions
- WW Temp and Flows
- Generalized Aerosol Emission Correlations

Introduction: Amine-Based CO₂ Capture

Pretreatment

Absorber

- Water
Amine
Emissions
1. Vapor
 2. Aerosol
- Fly ash
 - $\text{SO}_3 \leftrightarrow \text{H}_2\text{SO}_4$

Pretreatment
Inlet

Flue Gas

Pretreatment
Outlet

Amine
Solvent
Inlet

Inter-
cooling

Amine Solvent
Outlet

Water
Wash
Inlet

Water Wash
Outlet

Analytical Methods

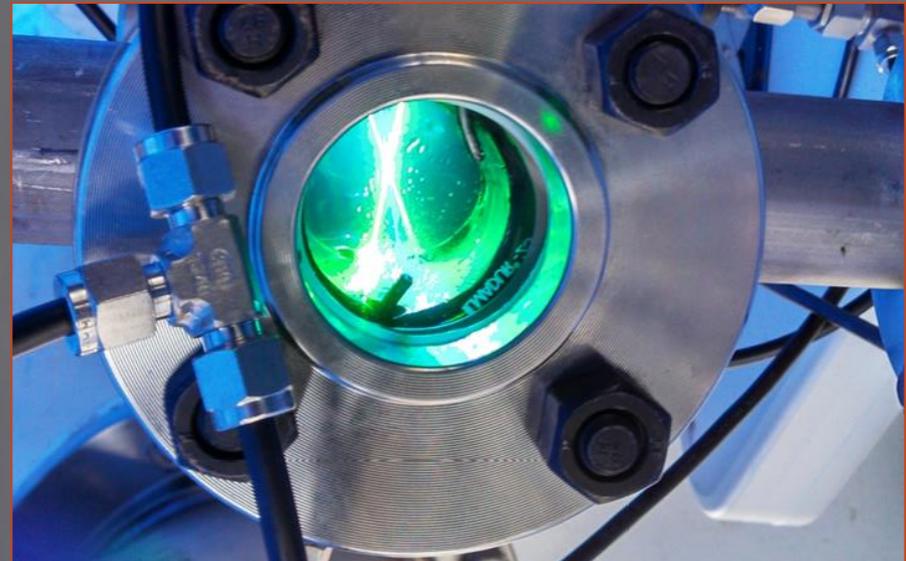
FTIR

- Gasmeter DX-4000
- Concentrations of H_2O , CO_2 , NH_3 , SO_2 , Amines
- No differentiating between vapor and aerosol phases

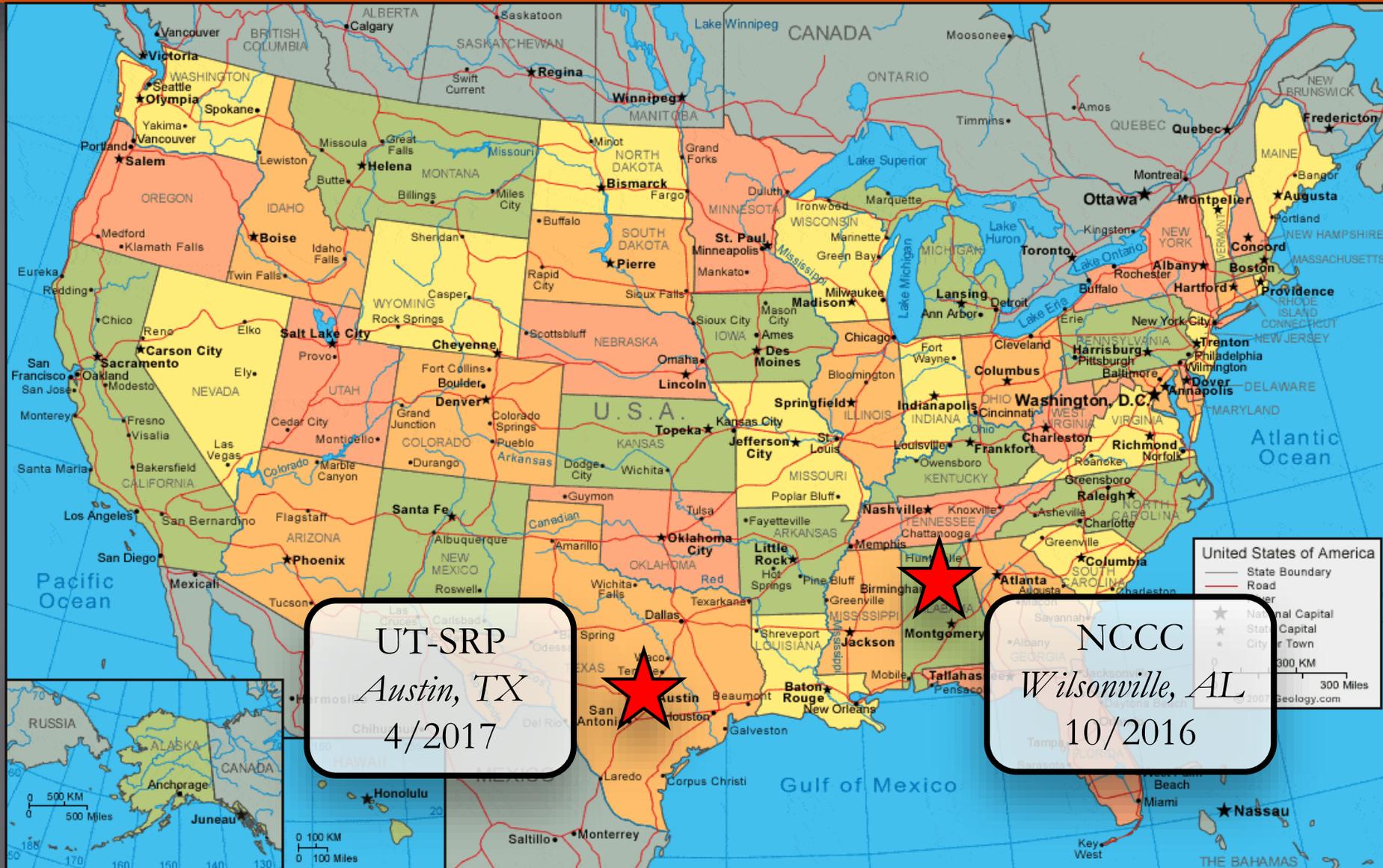


PDI

- Artium Technologies
- Drop sizes 0.1 to 12 μm
- Concentrations up to 10^7 per cm^3



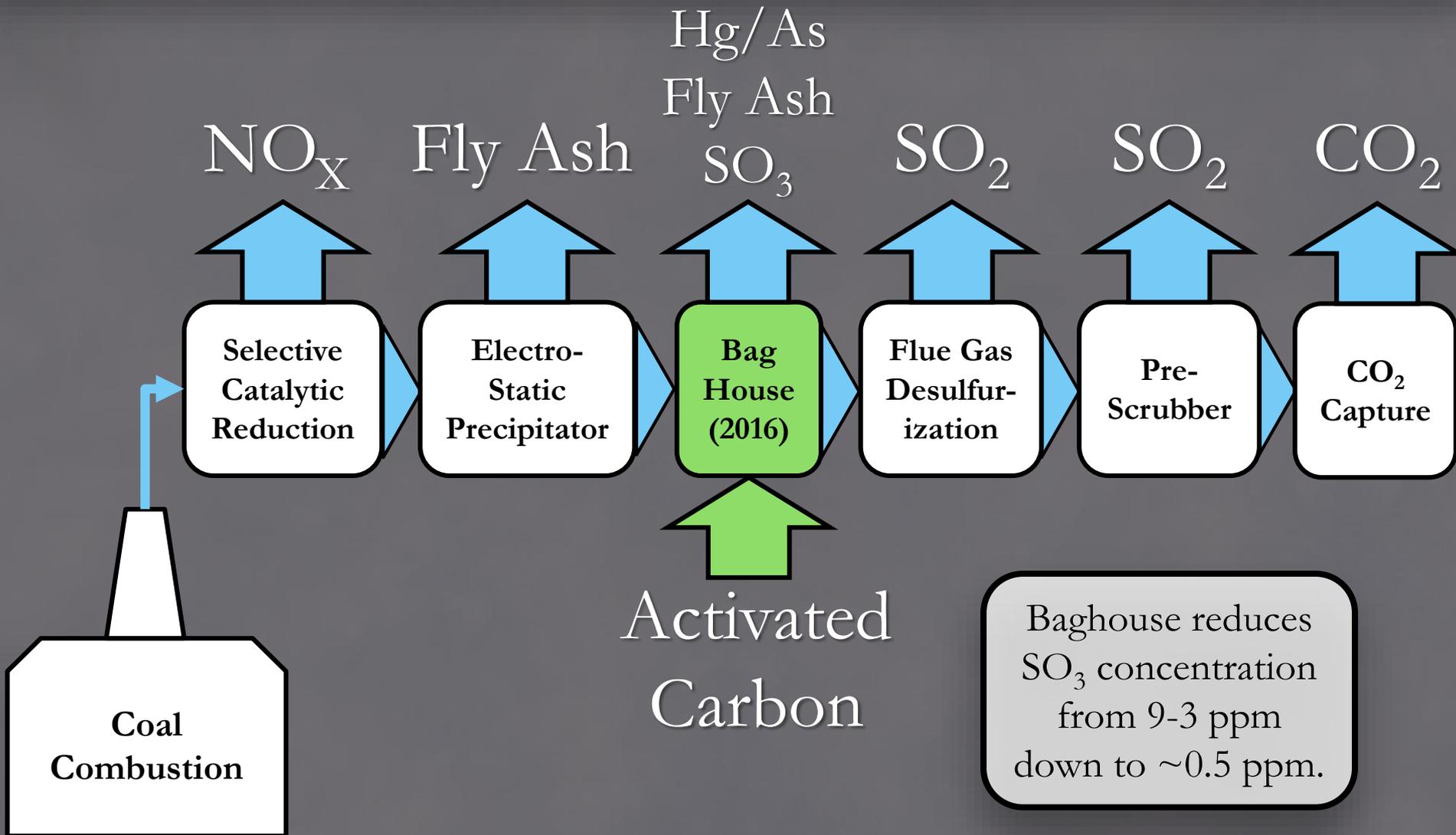
Amine Scrubbing Pilot Plant Sampling



Results

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Upstream Baghouse Flue Gas Treatment



Upstream Baghouse Flue Gas Treatment

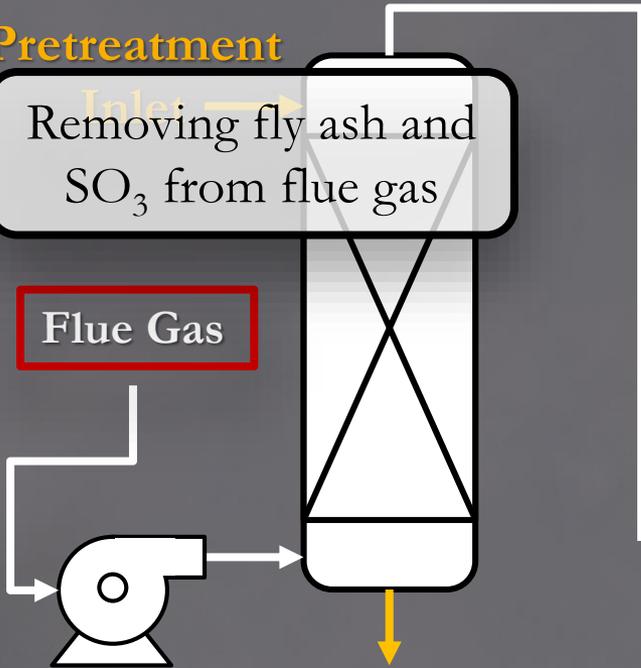
NCCC SSTU: 0.05 MWe
500 lb/hr

Pretreatment

Pretreatment

Removing fly ash and
 SO_3 from flue gas

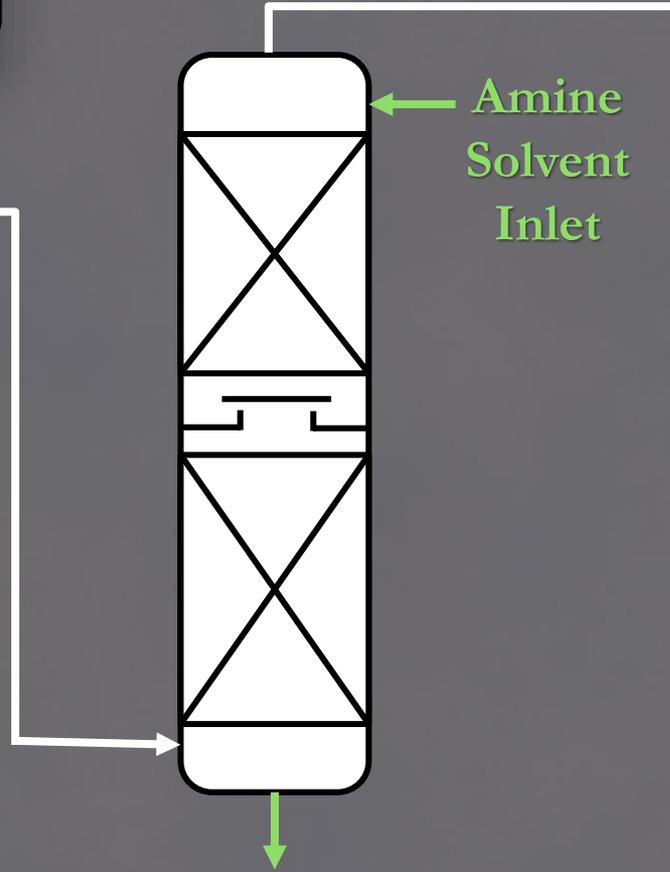
Flue Gas



Pretreatment
Outlet

Absorber

Amine
Solvent
Inlet

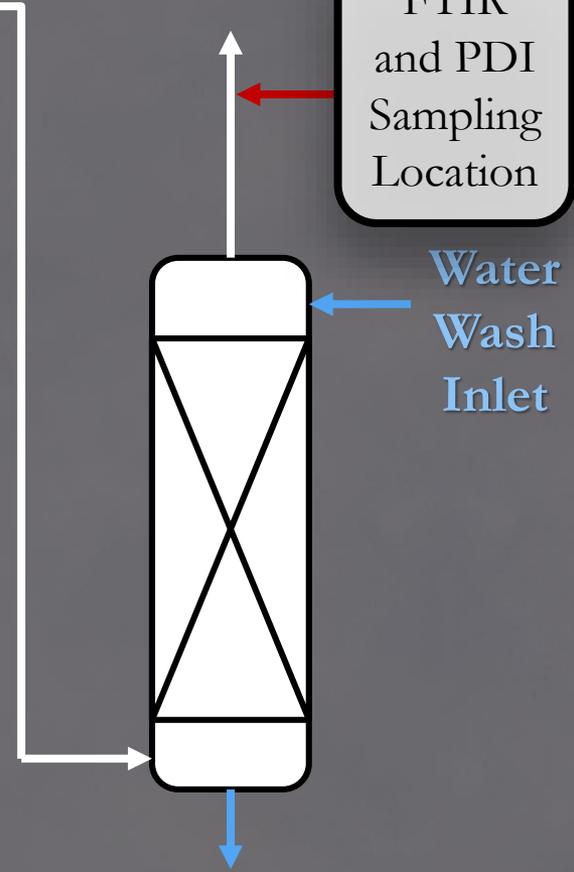


Amine Solvent
Outlet

Water Wash

FTIR
and PDI
Sampling
Location

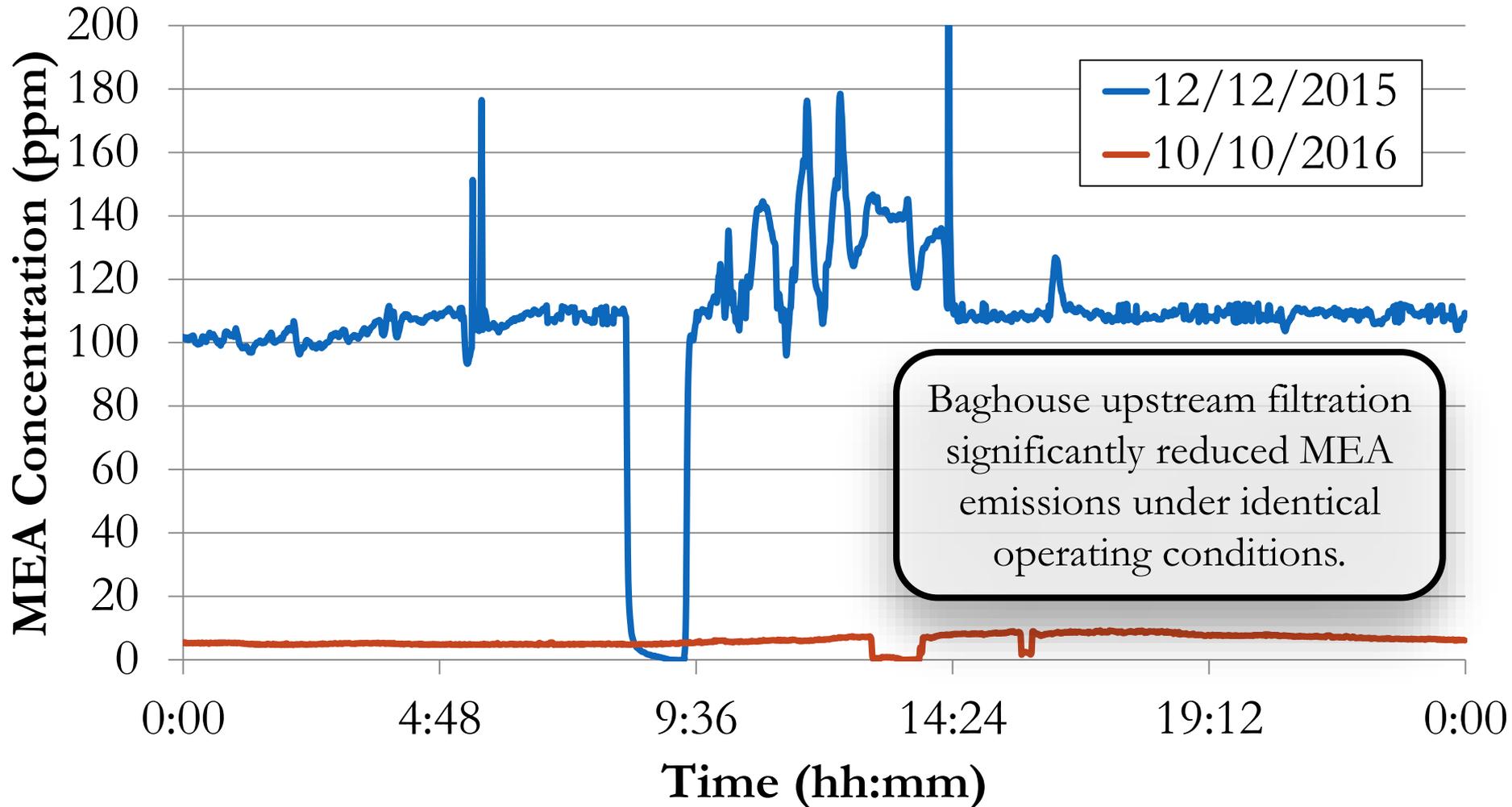
Water
Wash
Inlet



Water Wash
Outlet

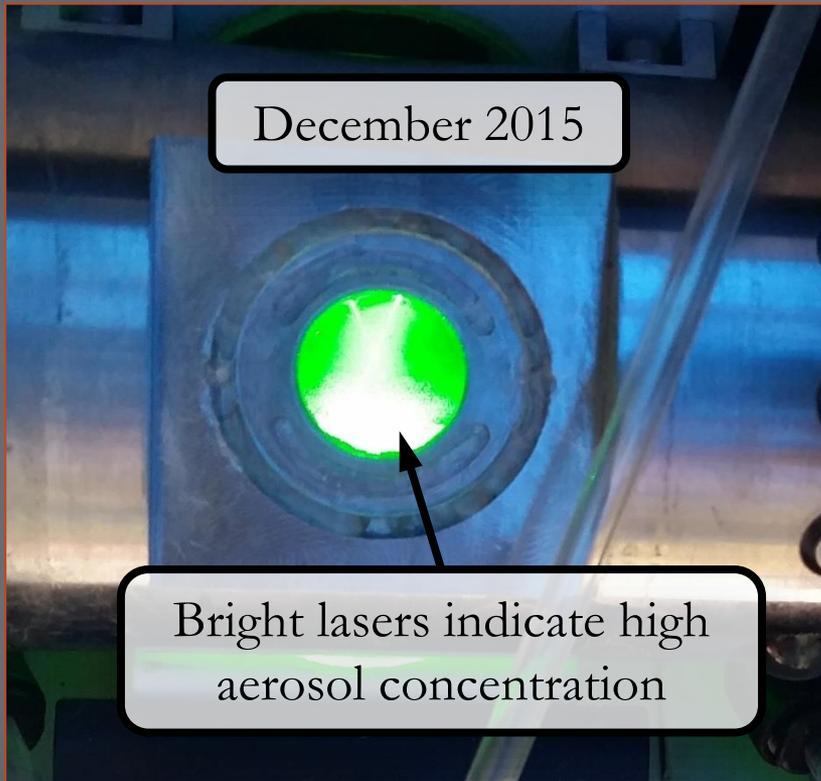
Upstream Baghouse Flue Gas Treatment

FTIR Sampling of MEA Emissions



Upstream Baghouse Flue Gas Treatment

PDI measurements on SSTU outlet:



Unable to detect aerosol at water wash outlet
($<0.1 \mu\text{m}$ diameter & low concentration)

SO₃ Generation at UT-SRP

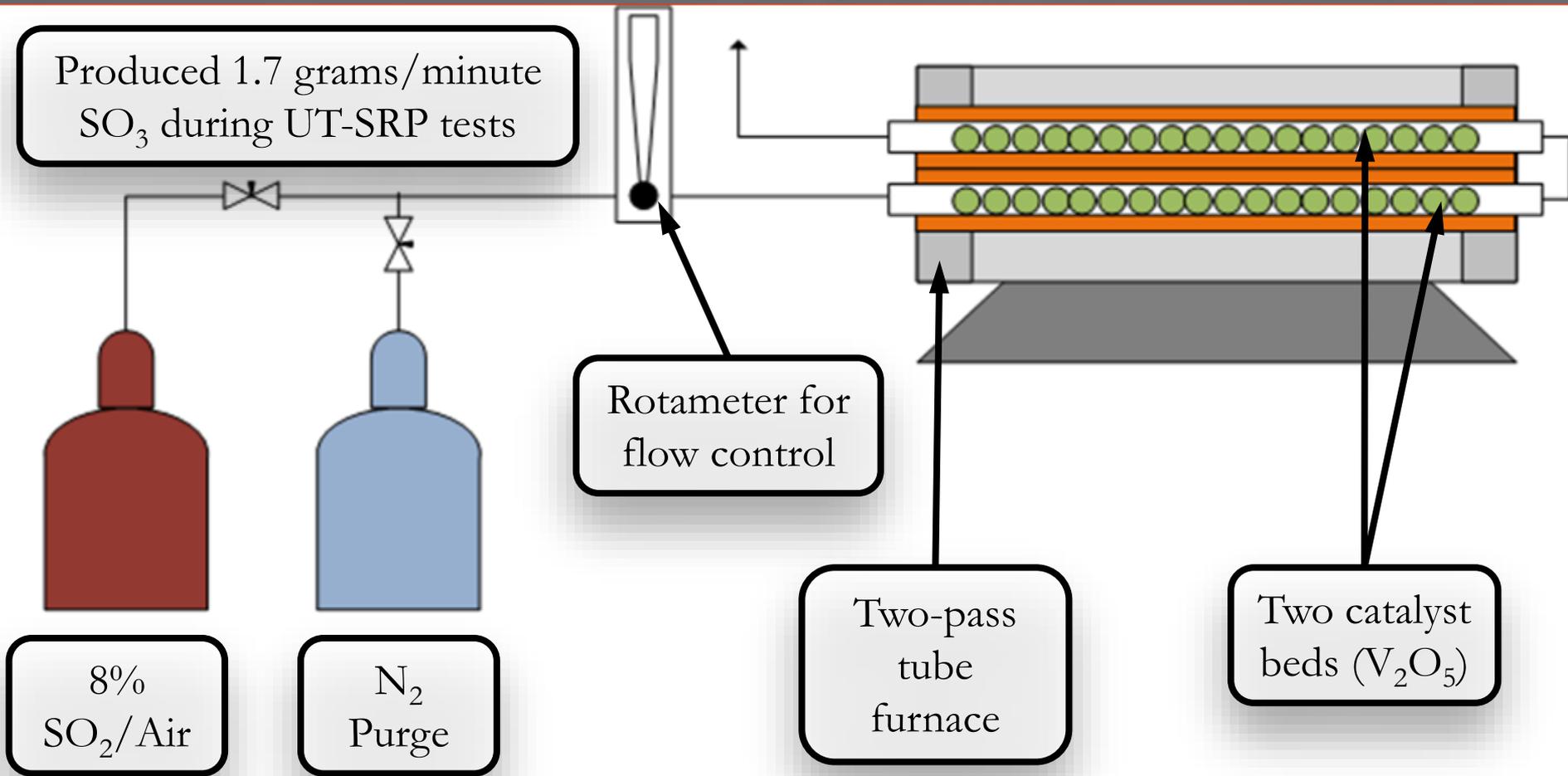
Baghouse is effective at aerosol mitigation

- Expensive solution
 - Will not be constructed at every facility
- Still need to improve understanding of how amine scrubbing process conditions impact aerosol emissions.

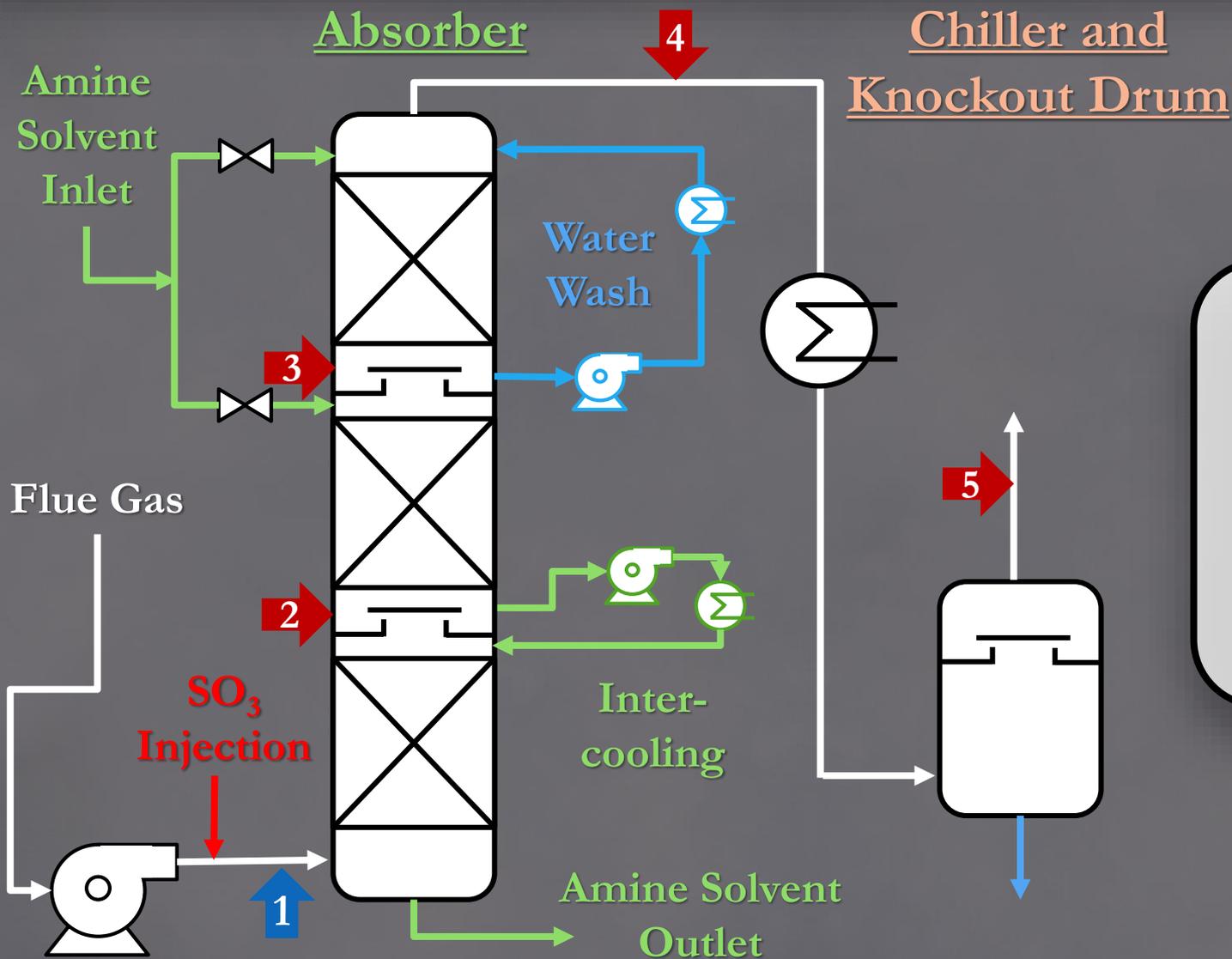
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SO₃ Generation at UT-SRP

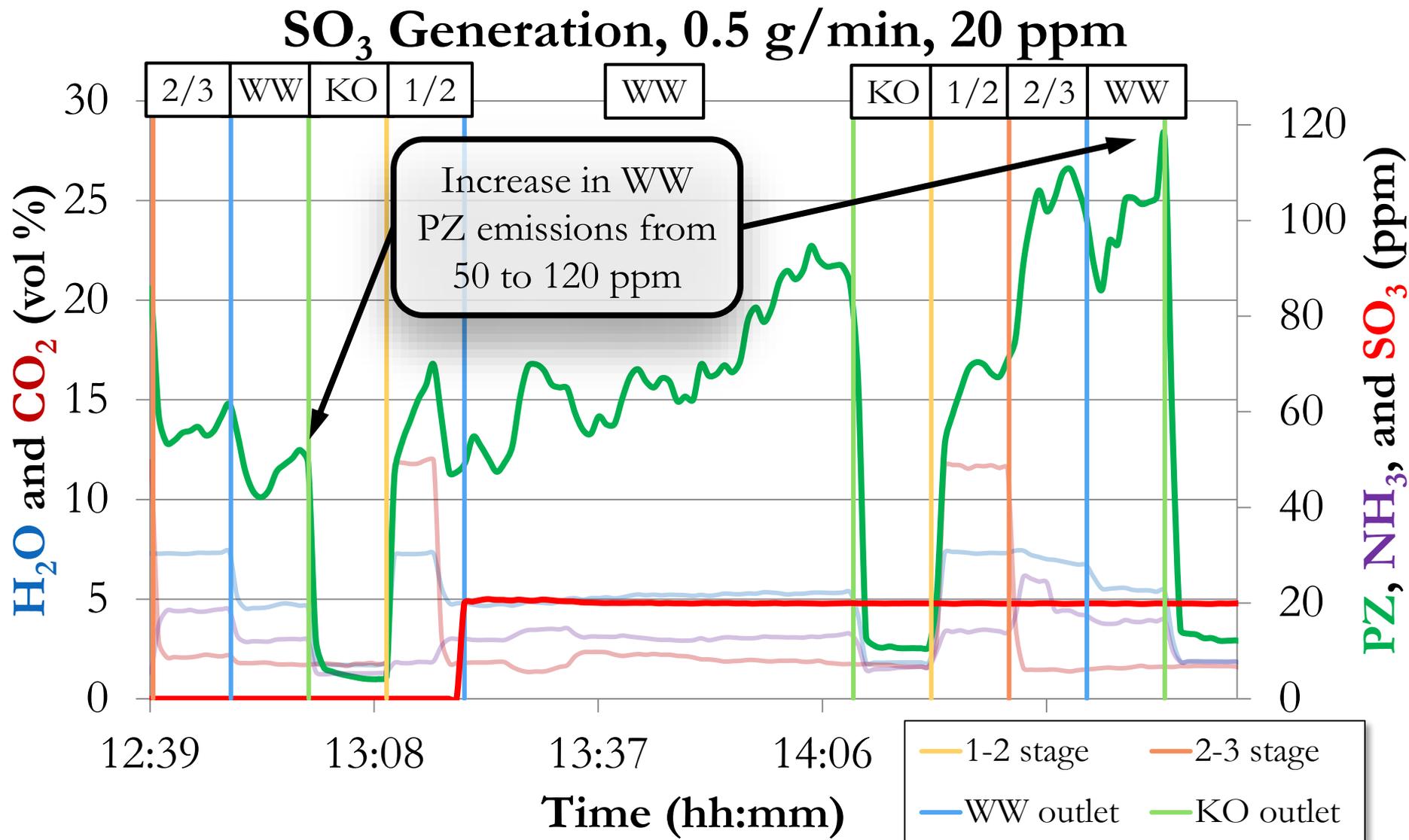


UT-SRP Pilot Plant: 0.1 MWe



5 Point FTIR
Sampling system:
(1) Inlet
(2) 1/2 Stage
(3) 2/3 Stage
(4) Outlet
(5) KO Outlet

SO₃ Generation and PZ Emissions



SO₃ Generation and PZ Emissions



SO₃ Generation and PZ Emissions

	Average	Min	Max
SO ₃ Concentration (ppm)	41	9	112
SO ₃ Generated (g/min)	0.84	0.23	1.68
SO ₃ Conversion Rate (%)	93.5	81.3	98.1
WW PZ Emissions with SO ₃ Injection	90	9	189
ppm PZ emitted per ppm SO ₃ injected	1.50	0.00	7.56

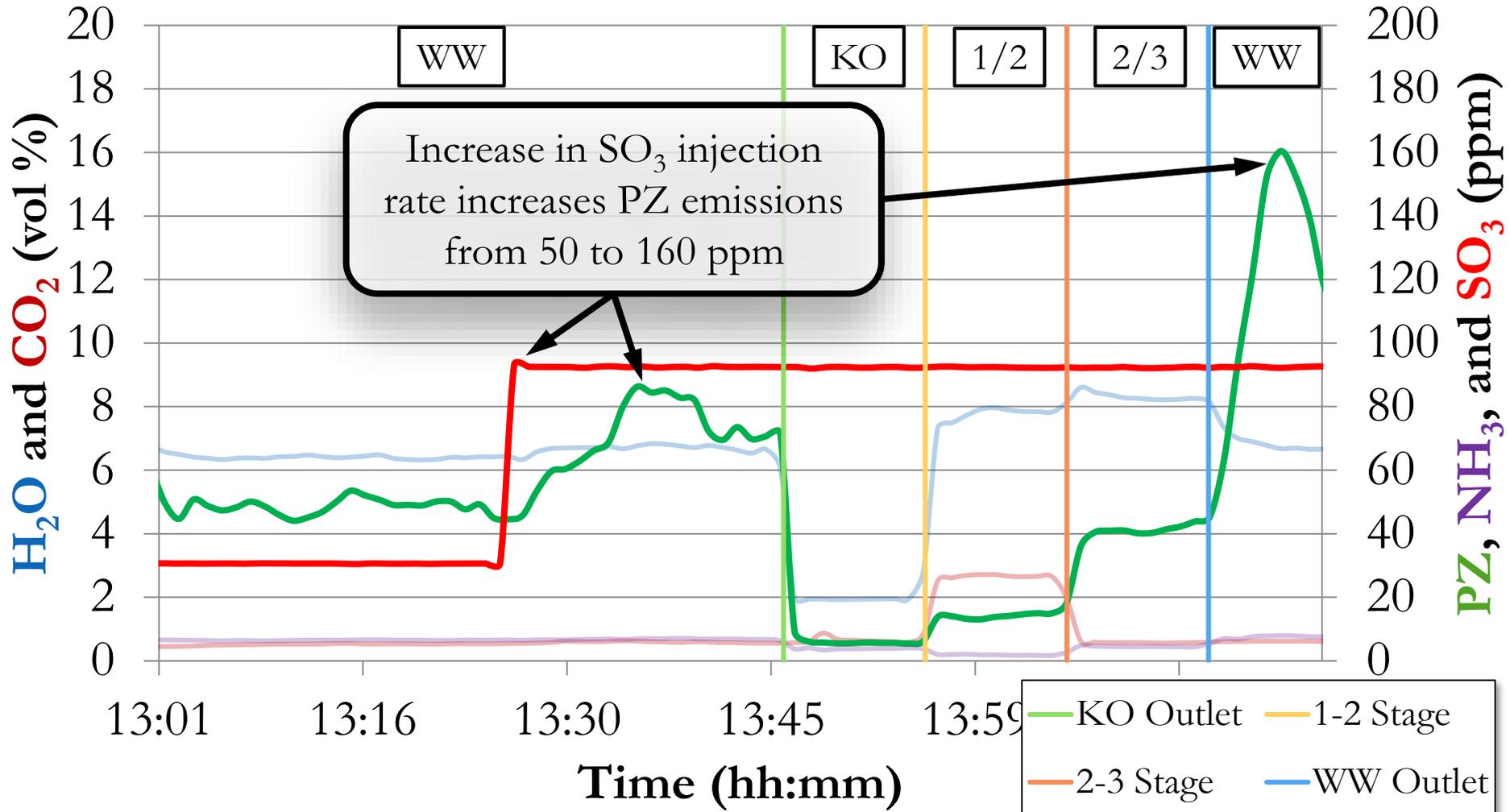
- 224 ppm for NCCC SSTU (0.05 MWe)
- 112 ppm for UT-SRP (0.1 MWe)
- 22 ppm for NCCC PSTU (0.5 MWe)

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Water Wash Effect on PZ Emissions

SO₃ Generation, 0.5 → 1.4 g/min, 31 → 92 ppm

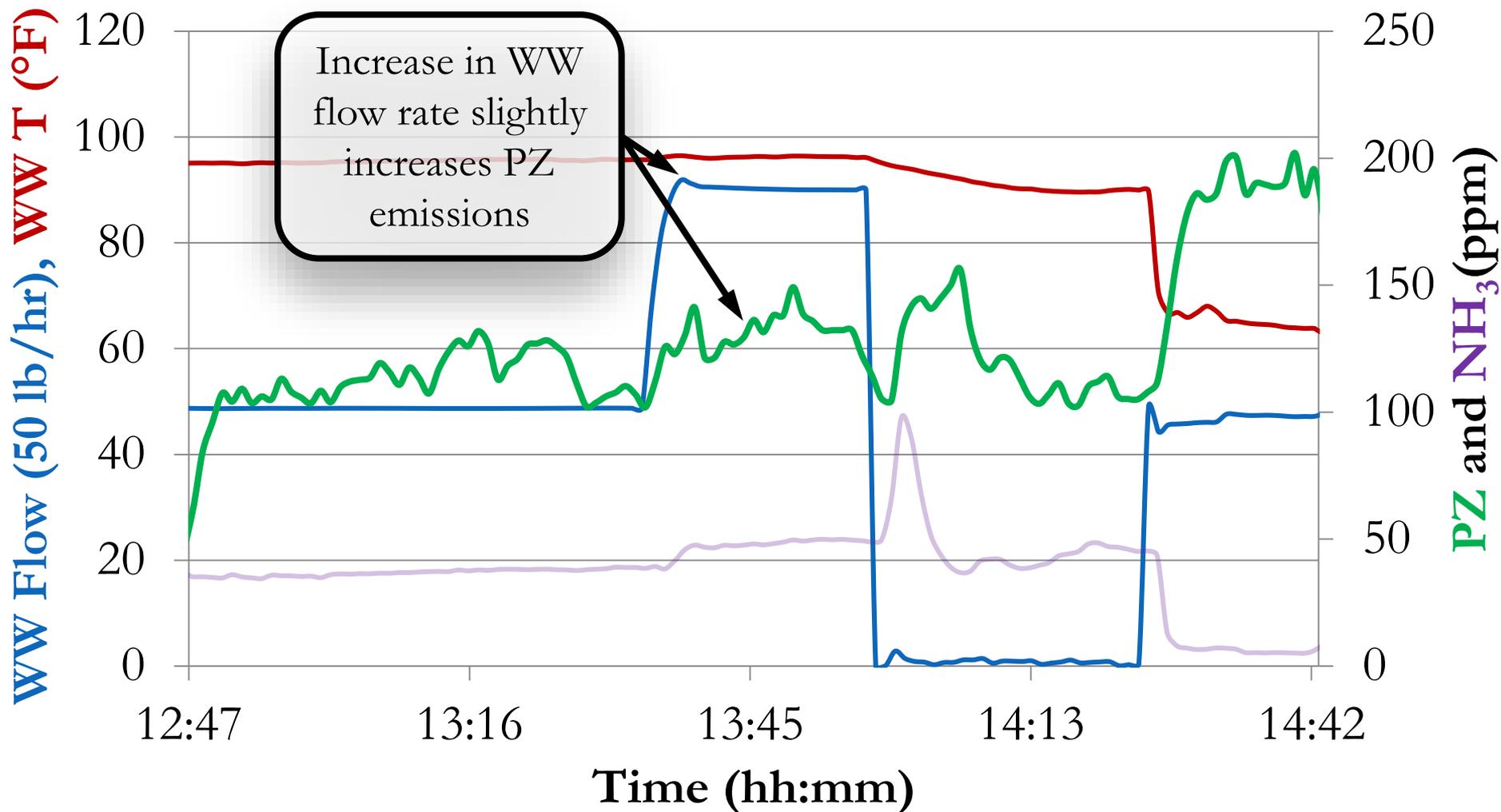


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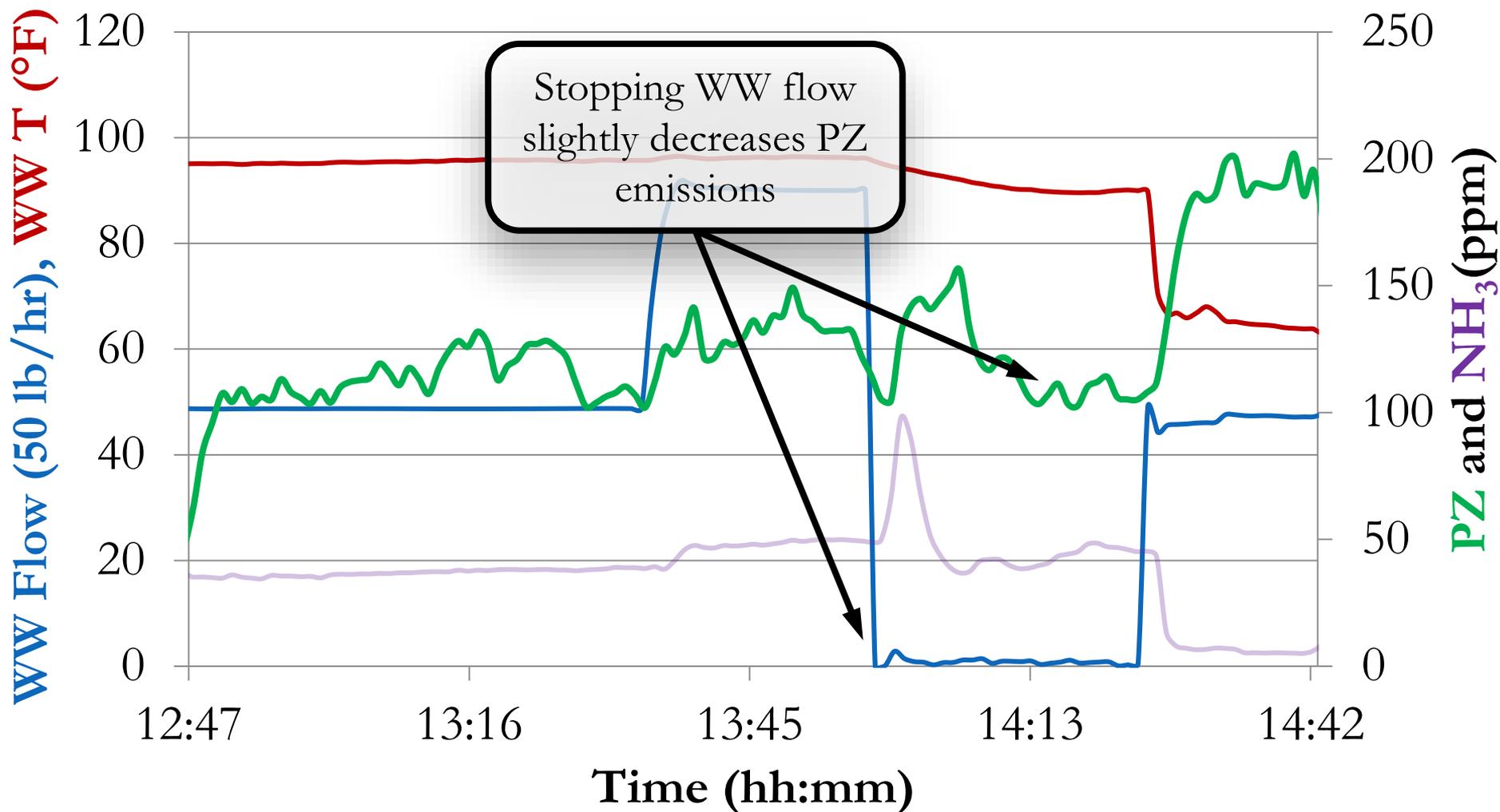
Water Wash Effect on PZ Emissions

SO₃ Generation, 1.4 g/min, 53 ppm



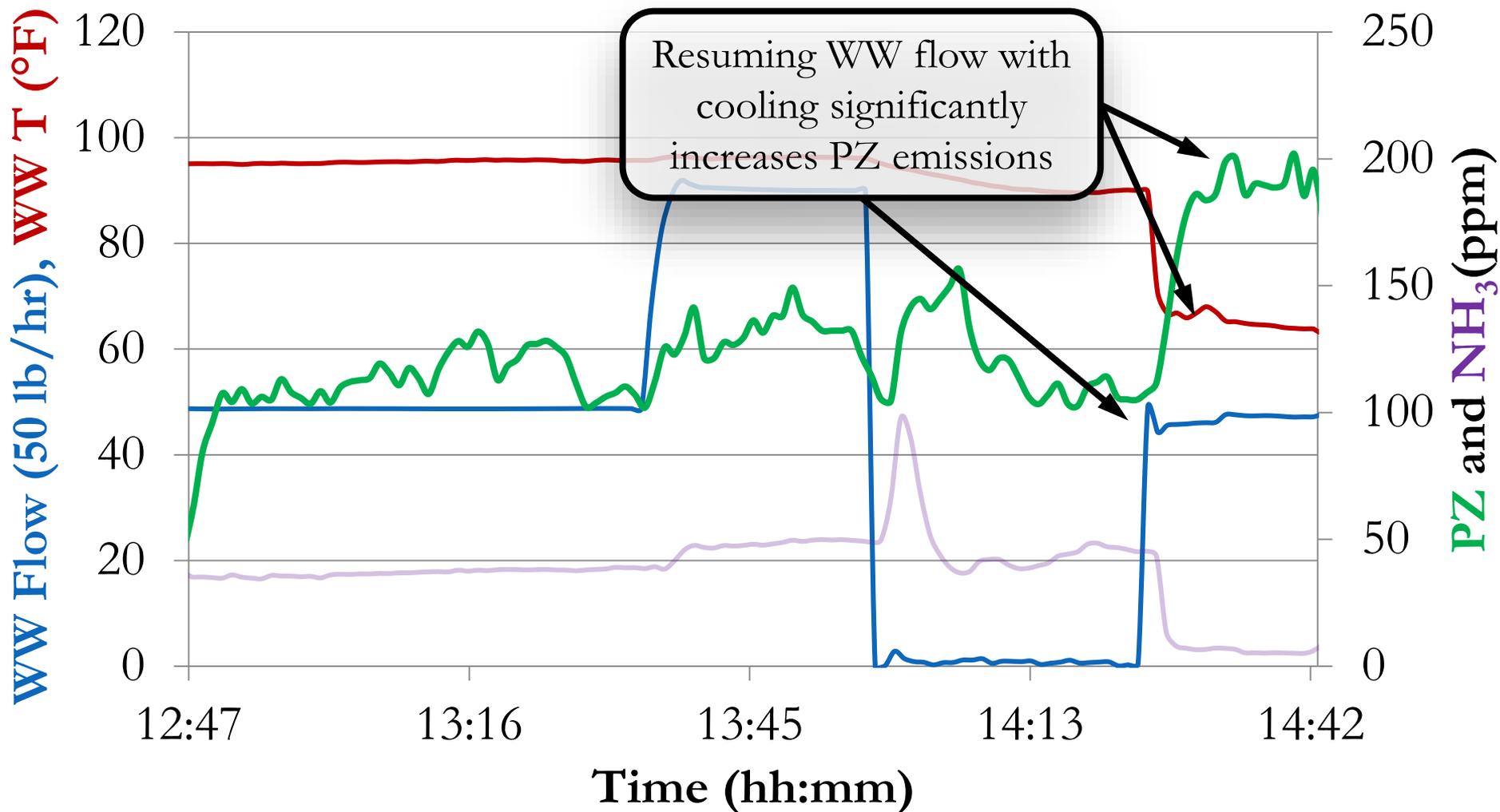
Water Wash Effect on PZ Emissions

SO₃ Generation, 1.4 g/min, 53 ppm



Water Wash Effect on PZ Emissions

SO₃ Generation, 1.4 g/min, 53 ppm



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Aerosol Emission Correlations

- Analysis of process properties to observe how each impacts aerosol emissions:
 - Temperatures
 - Flow Rates
 - Gas Phase Concentrations

Aerosol Emission Correlations

Temperatures:	R ²
Gas Outlet T	0.564
Top Solvent/WW T	0.493
IC Solvent T	0.118
Top Bed T	0.510
Middle Bed T	0.172
Bottom Bed T	0.107

- Temperatures at top bed have greater correlation with amine emissions than lower bed temperatures.
- Amine emissions depend on gas temperatures more than solvent temperatures.

Aerosol Emission Correlations

Flow Rates	R ²
Water Wash Flow	0.397
Intercooling Flow	0.206
L/G	0.162

- Solvent flow rates at top beds have a greater impact on amine emissions than flow rates through lower beds

Aerosol Emission Correlations

Gas Phase Concentrations	R ²
CO ₂ In	0.143
CO ₂ Out	0.270

- CO₂ concentration at absorber outlet has greater correlation with amine emissions than CO₂ concentration at inlet

Conclusions

- Baghouse pretreatment mitigates amine aerosol at NCCC.
- Increasing SO_3 concentrations increases amine emissions.
- Process temperatures most significant in determining aerosol emissions.
 - Gas temperatures matter more than solvent temperatures.
 - Temperatures at absorber outlet more significant than temperatures at the inlet.
- Solvent emissions more dependent on water wash flow rates than intercooling/lower bed flow rates.
- Increasing CO_2 concentration at absorber outlet decreases amine aerosol emissions.

Acknowledgements

Thank you

- Rochelle Lab
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 - Dr. Eric Chen
 - Korede Akinpelumi and Vietnam Nguyen
- NCCC SSTU operations crew
- UT-SRP operations crew



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References

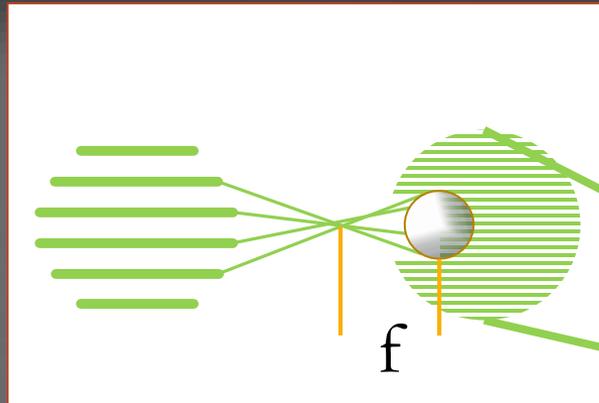
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- Saha C., Irvin J. H. “Real-time aerosol measurements in pilot scale coal fired post-combustion CO₂ Capture.” *Journal of Aerosol Science*. 2017;104:43-57

Additional Slides

Analytical Methods: PDI

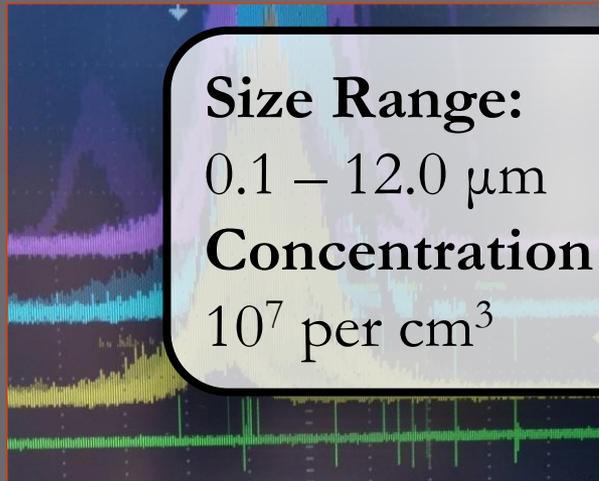
Photodetectors quantify drop size via phase shift

- Reduces window attenuation



Droplet movement causes Doppler shift in phases

- Determines droplet velocity



Size Range:

0.1 – 12.0 μm

Concentration Limit:

10^7 per cm^3

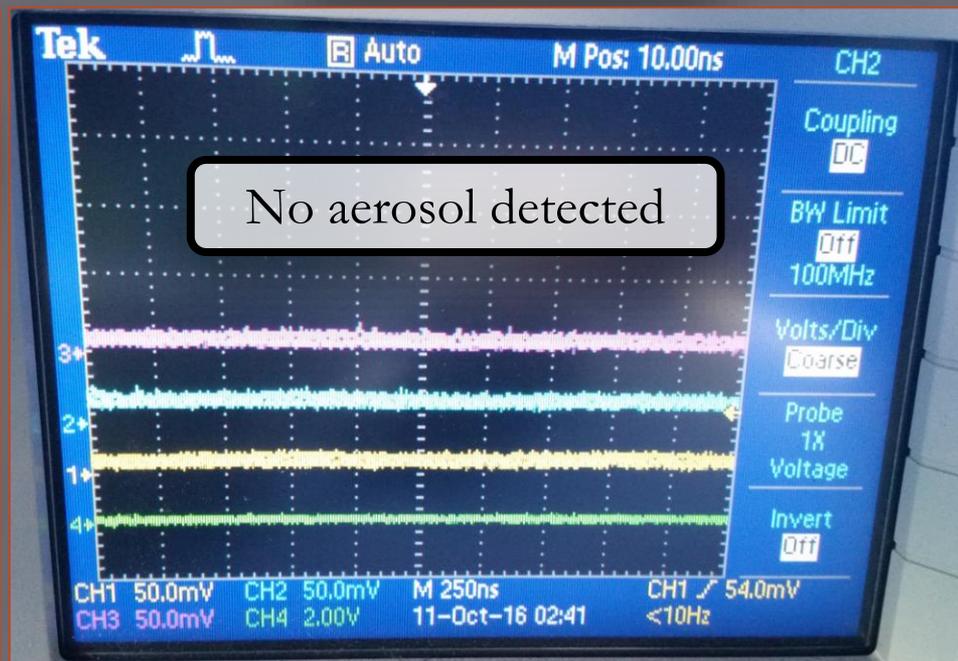
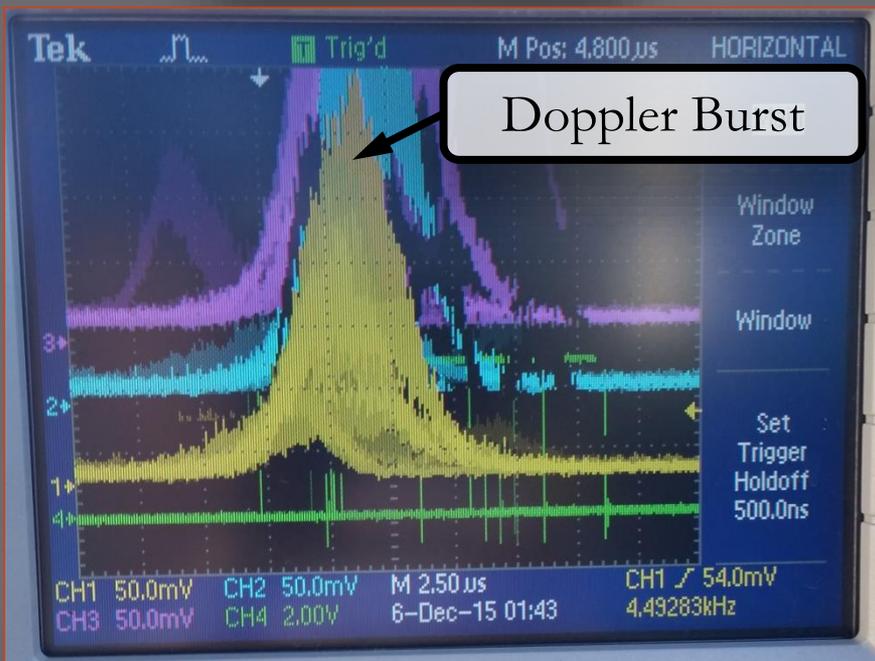
Velocity + number count used to determine particle concentration

Upstream Baghouse Flue Gas Treatment

PDI measurements on SSTU outlet:

December 2015

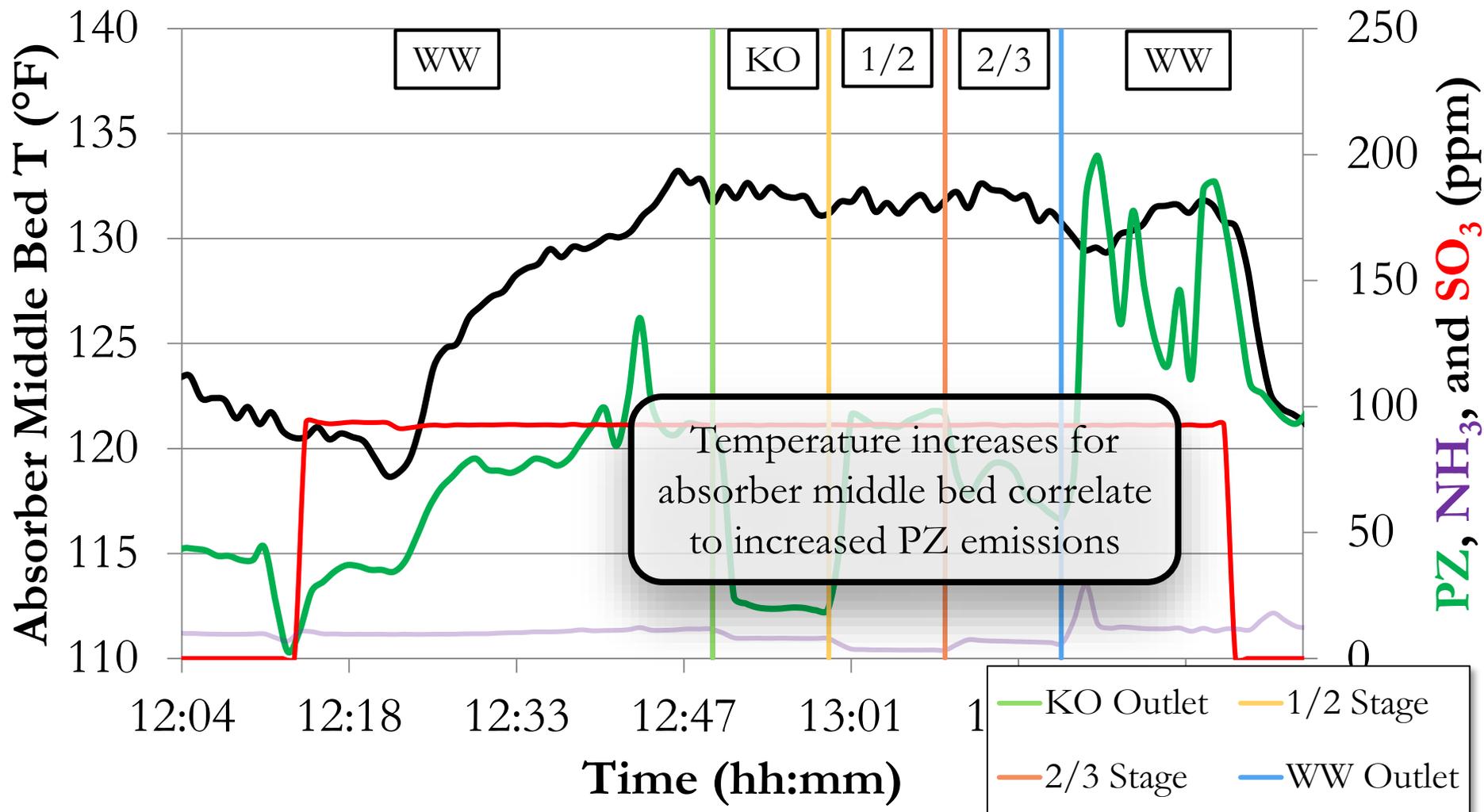
October 2016



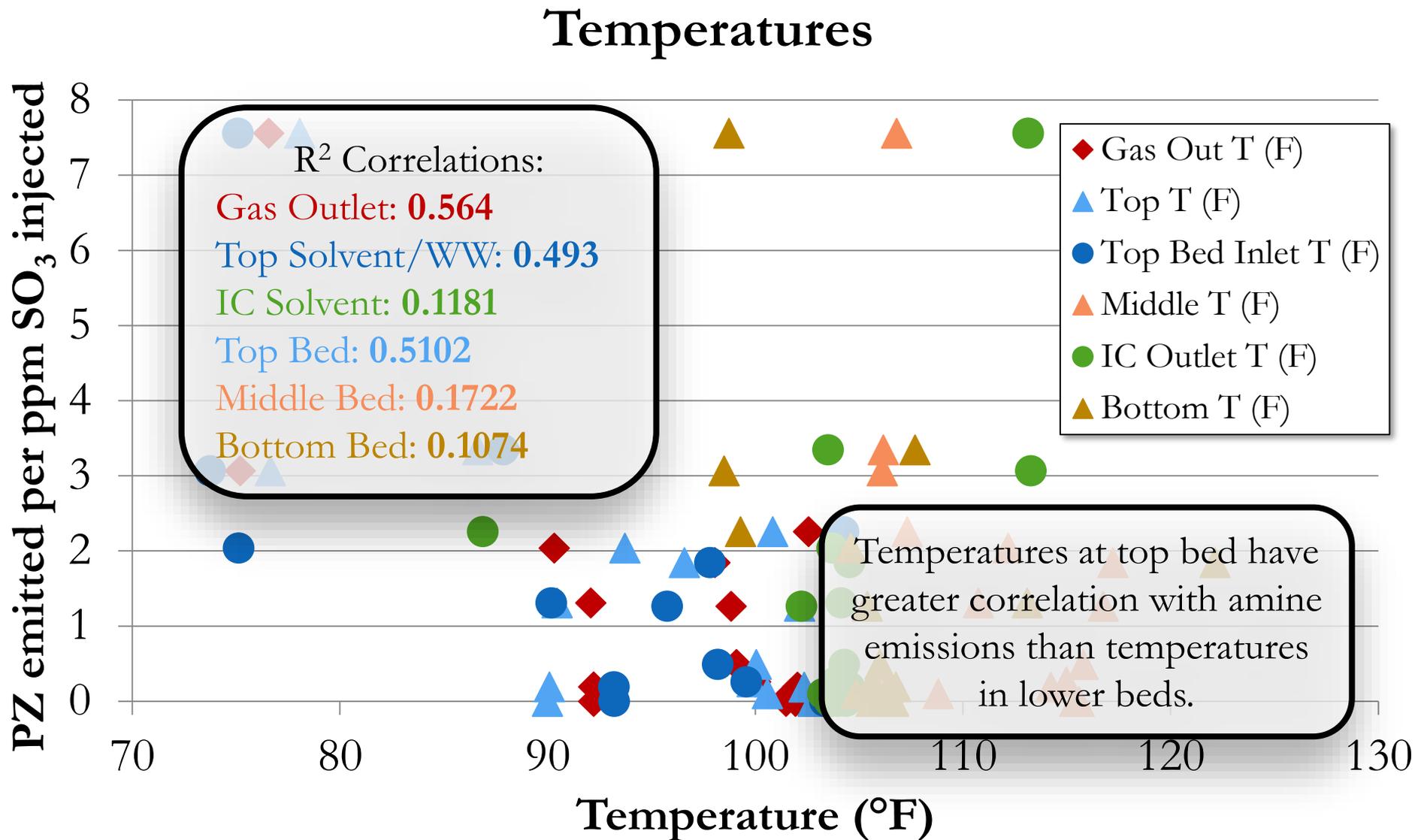
Lack of aerosol confirmed with oscilloscope

Absorber T Effect on PZ Emissions

SO₃ Generation, 1.4 g/min, 93 ppm

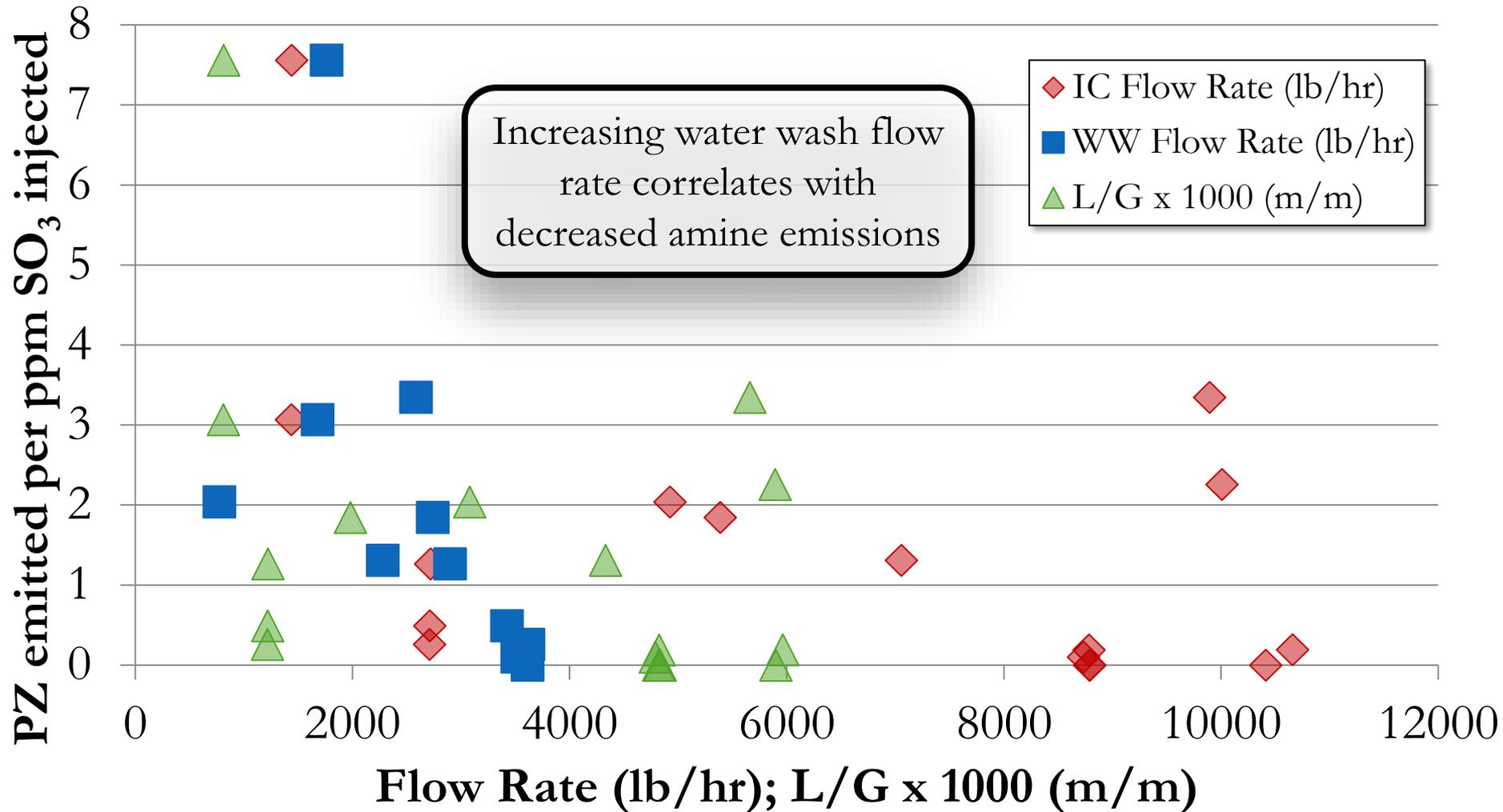


Aerosol Emission Correlations



Aerosol Emission Correlations

Flow Rates



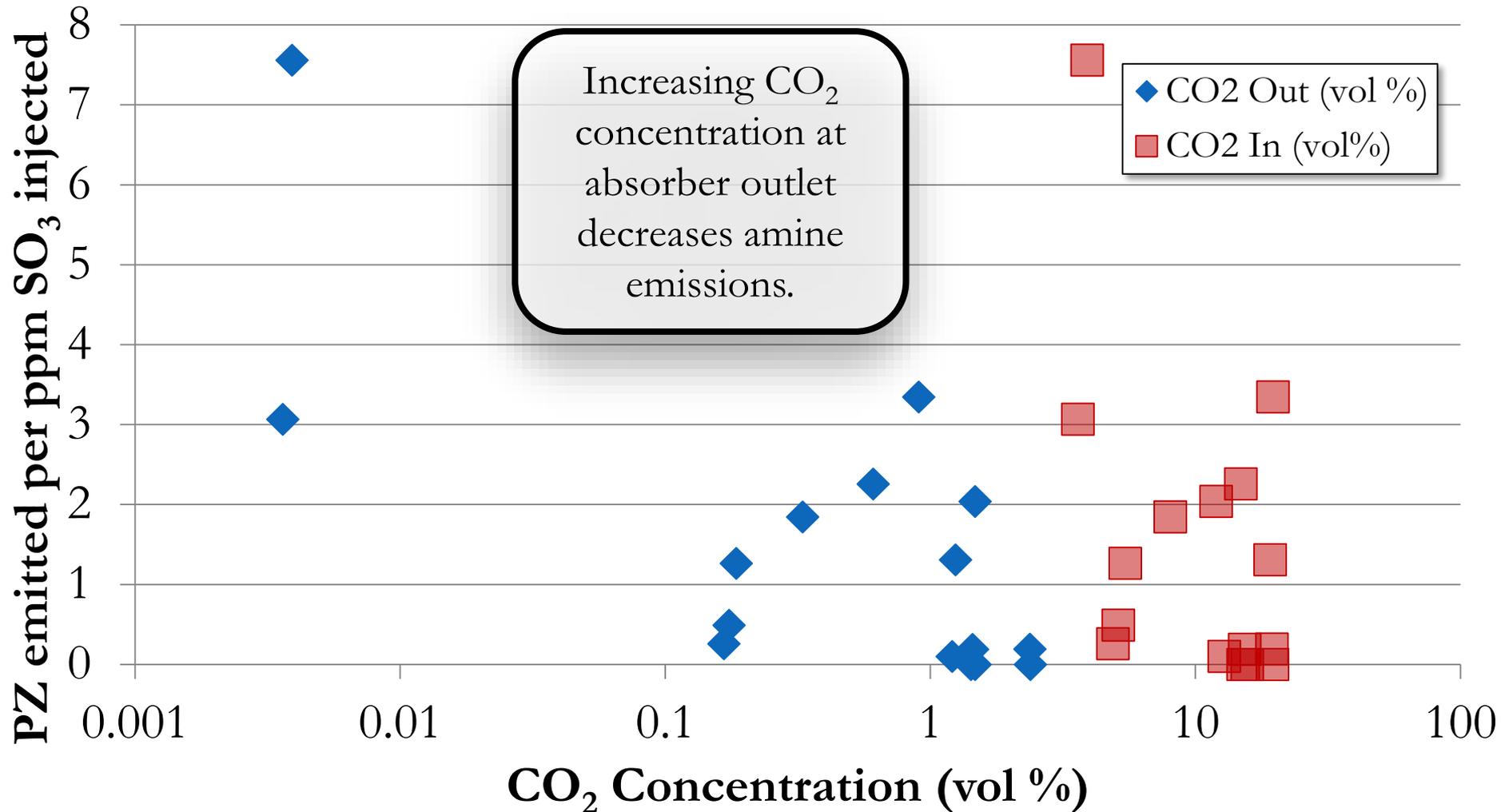
Aerosol Emission Correlations

Solvent Loadings	R ²
Rich Loading	0.367
Lean Loading	0.005

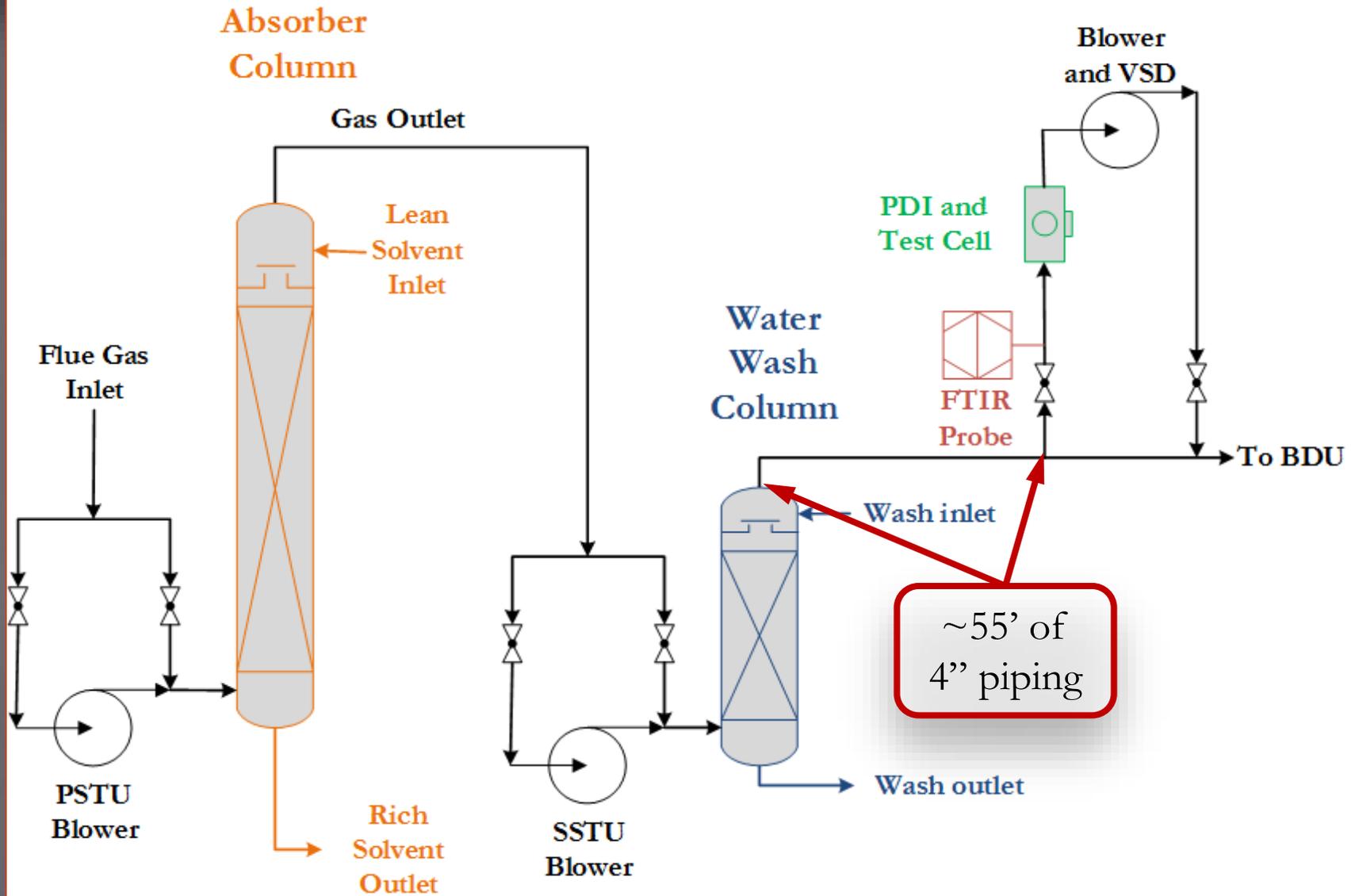
- Rich loading has greater influence on amine emissions than lean loading

Aerosol Emission Correlations

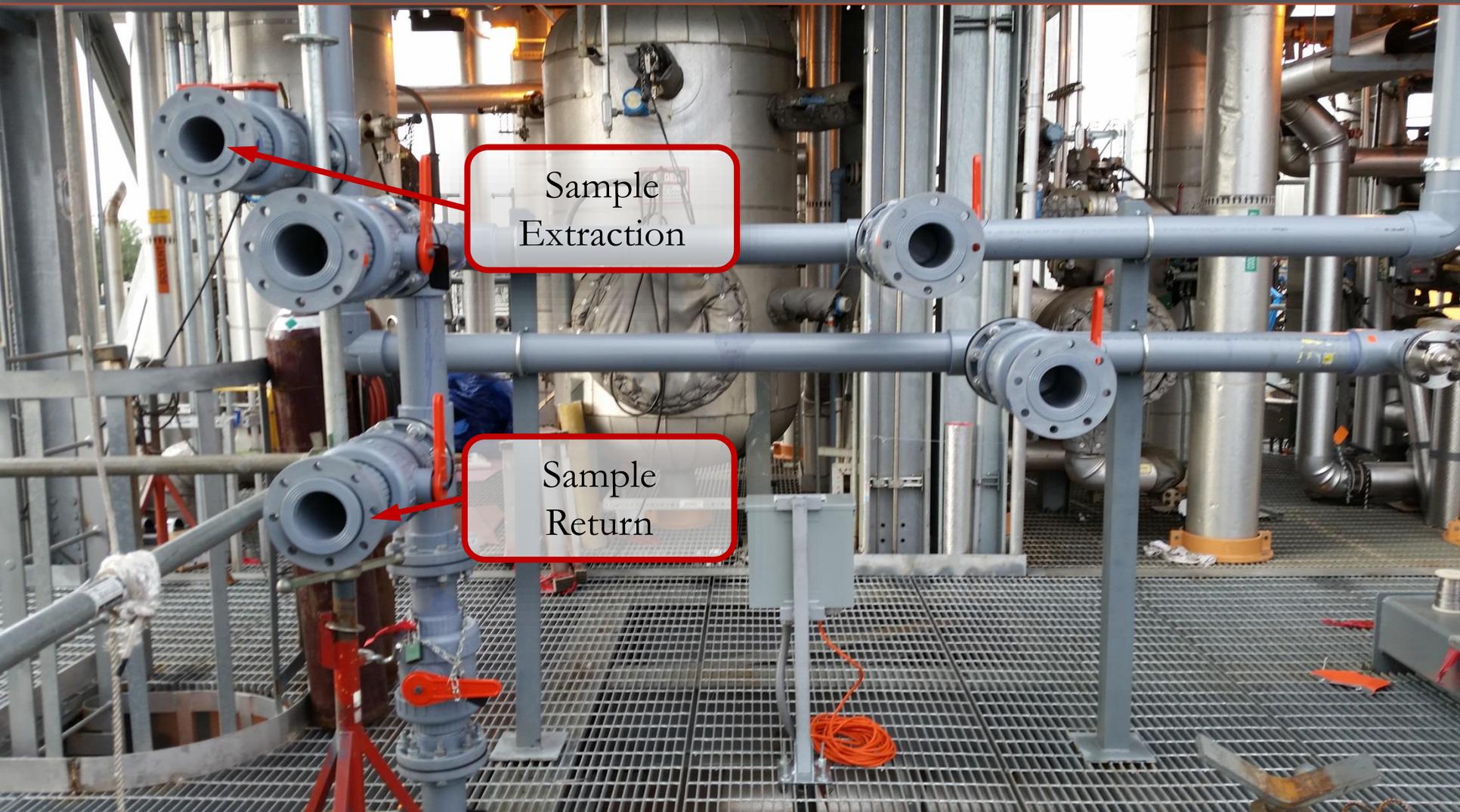
Inlet and Outlet CO₂ Concentrations



NCCC SSTU



FTIR and PDI Field Sampling



FTIR and PDI Field Sampling

